

# Development of evaporation and melting models for meteor phenomenon in the continuum regime

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Annual BRAIN-BE meeting : METRO  
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# The meteor phenomena ... inspiration for space exploration



Artistic View Meteor [MidnightWatcher's]

**50 -100 tonnes of meteor enter in the earth's atmosphere per day**

- **Velocity** : 11.2 - 72.5 km/s
- **Composition**: FeO; MgO; Ca; SiO<sub>2</sub>, ...
- **Size**: radius 1 μm – 10 m

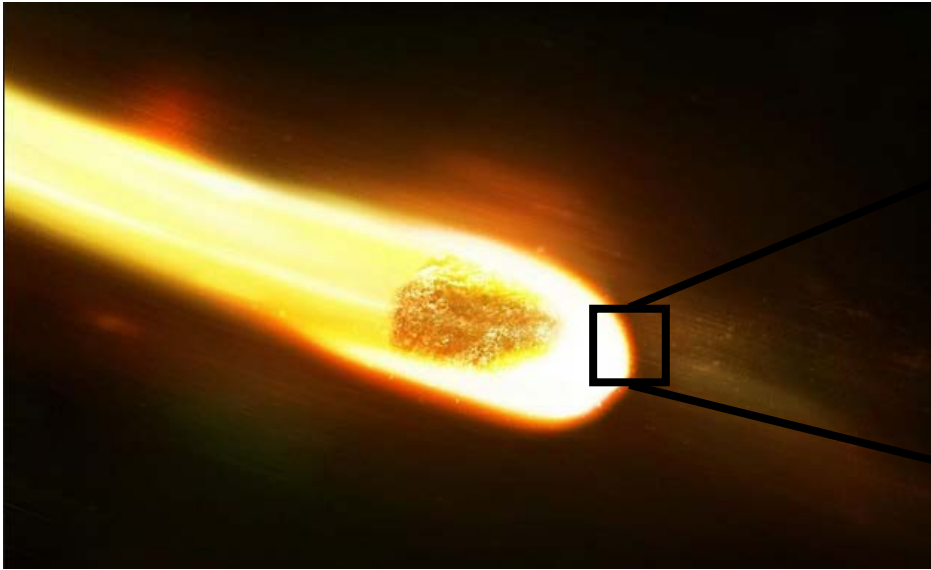


Artistic illustration of the Apollo's re-entry (NASA)

**Meteor ablation source of inspiration for ablative heat shields**

- **Velocity** : 7.9 - 14 km/s
- **Composition TPS**: C(gr), SiO<sub>2</sub>, C<sub>6</sub>H<sub>5</sub>-OH
- **Size**: radius 0.5 m – 2 m

# The meteor phenomena ... it melts (heat shields don't)



Artistic View Meteor [MidnightWatcher's]



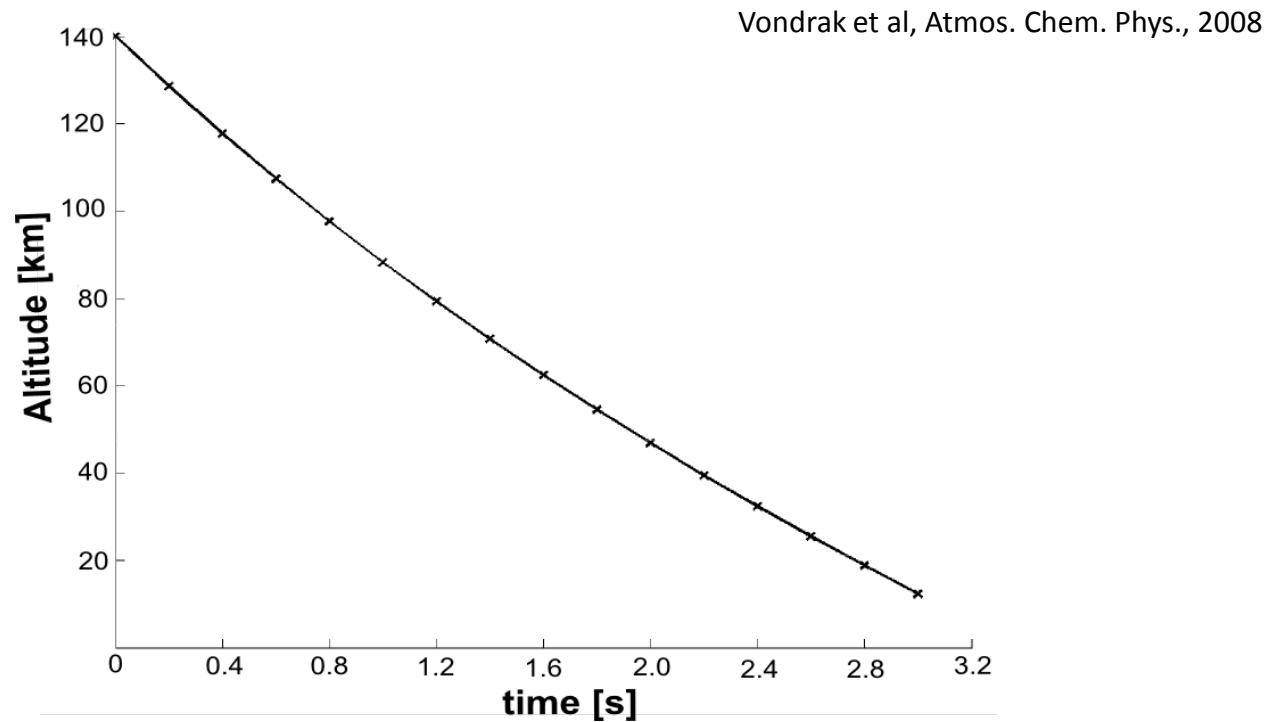
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**Oxides at high temperatures**  
(surface temperature > fusion temperature)

# State-of-the-art model for meteor entry phenomena

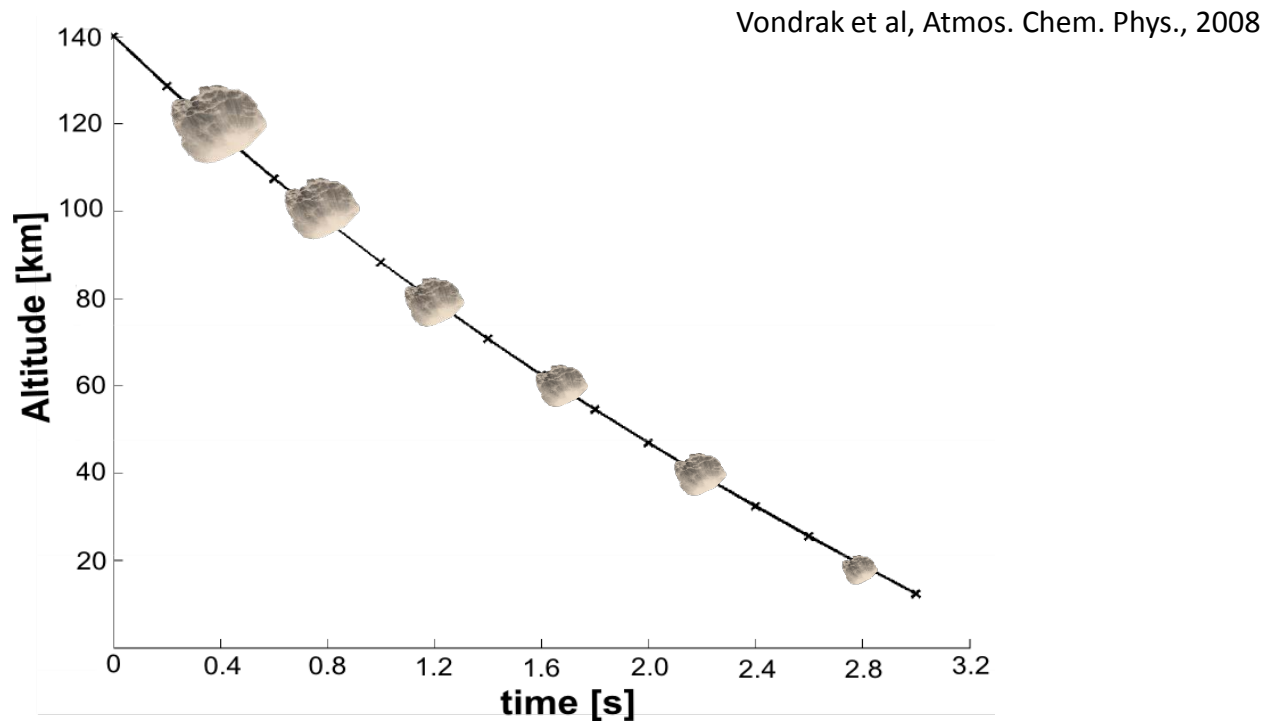
Trajectory: 
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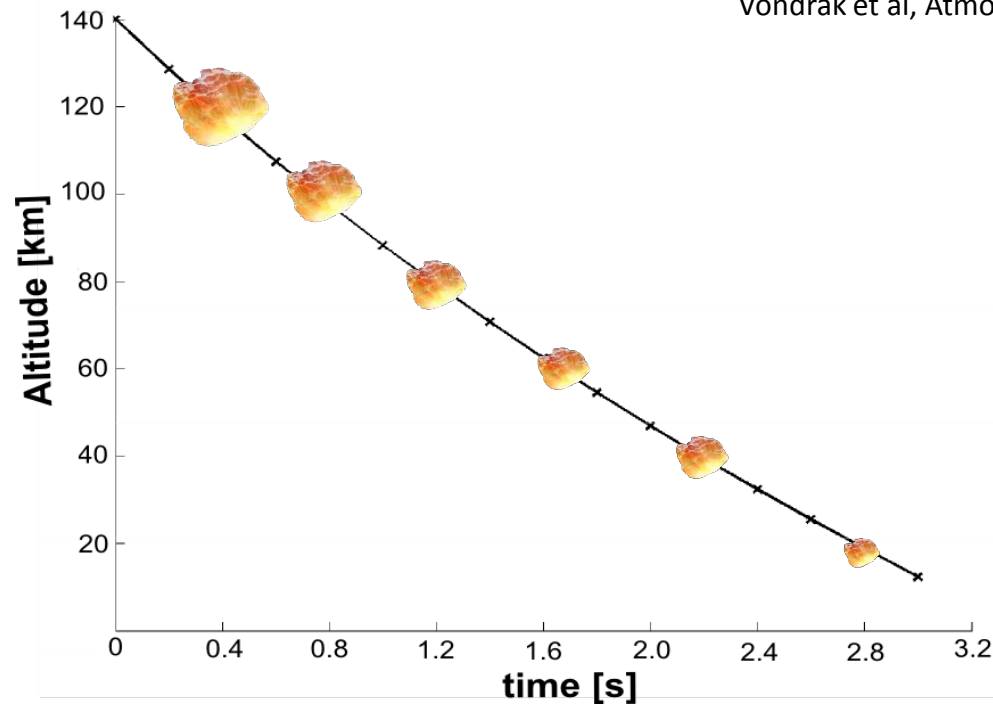
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Vondrak et al, Atmos. Chem. Phys., 2008



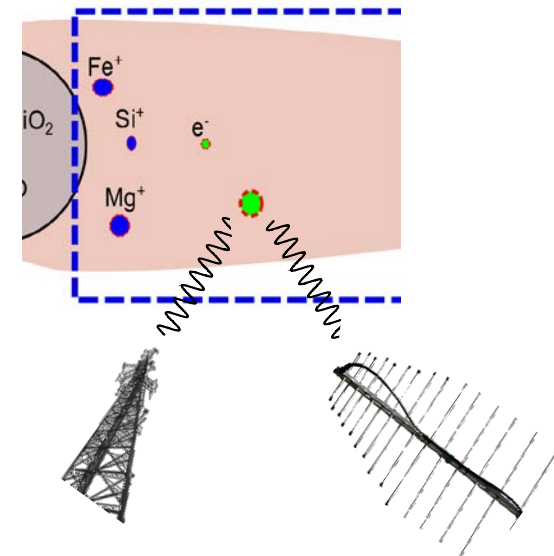
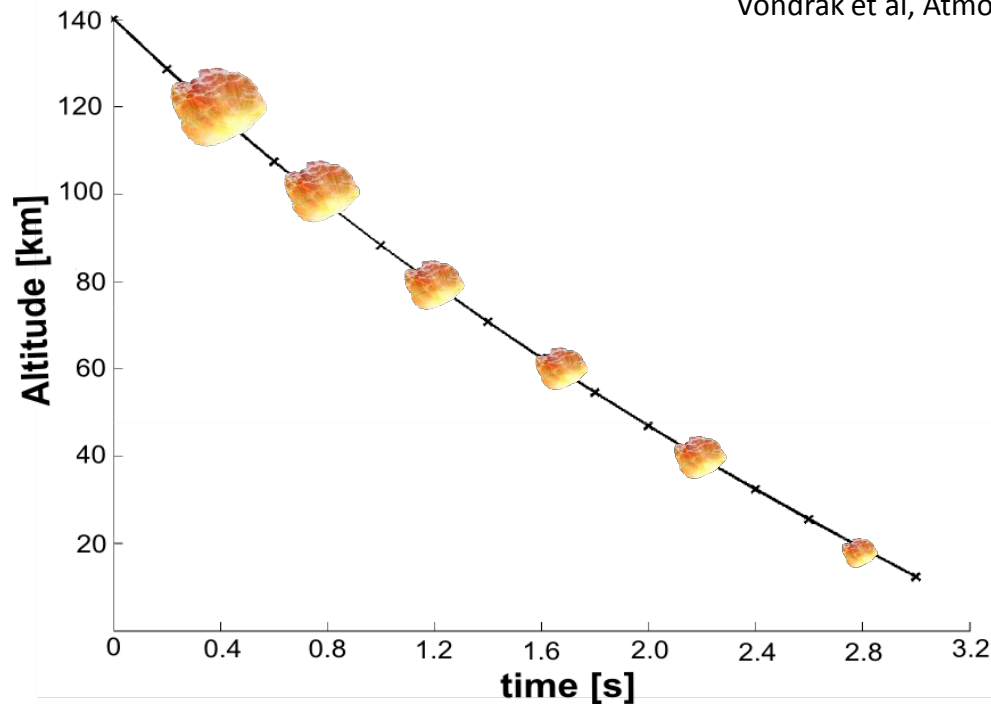
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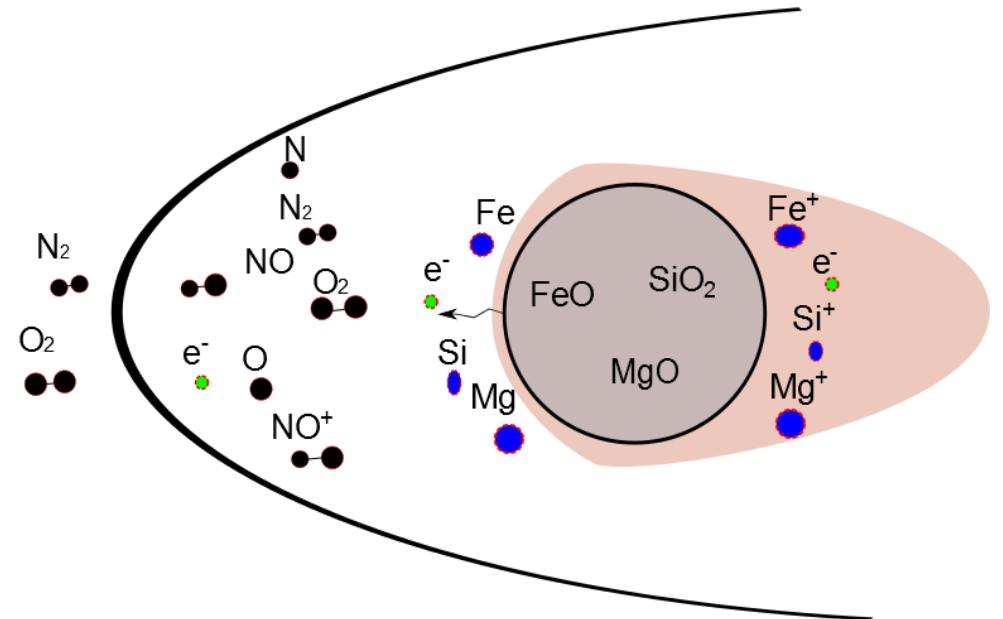
**no prediction of the electron concentration**

# Objectives

Detailed flow analysis during a meteor entry based on an aerospace engineering approach including melting

Focus of the study:

- Continuum flow
- Single fragment meteor
- Geometry: sphere
- Forward stagnation streamline





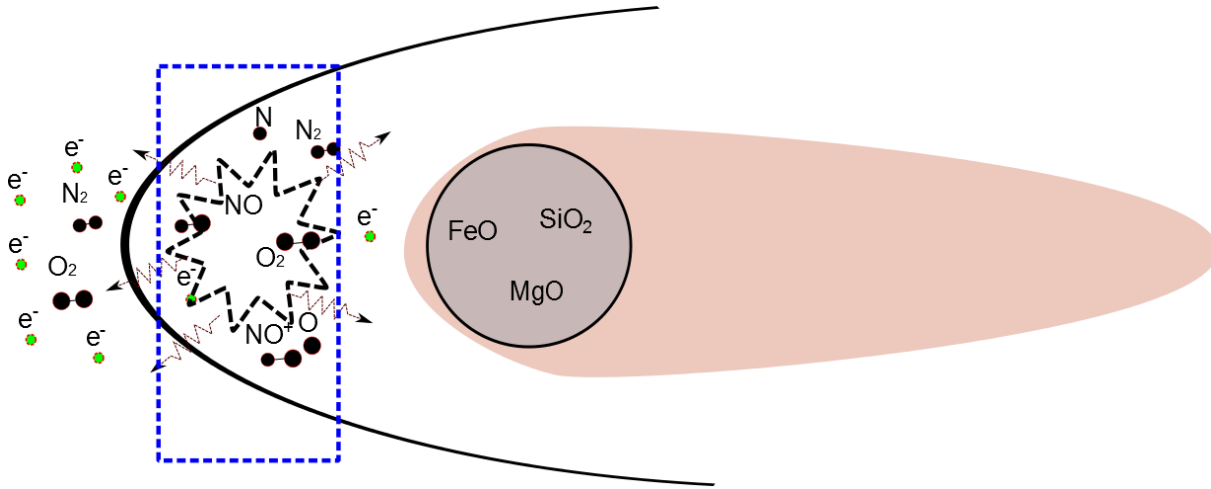
# Outline

- Flow field Modeling
- Gas-surface interaction modeling for meteors
- Numerical tools & results
- Conclusion and Future Work

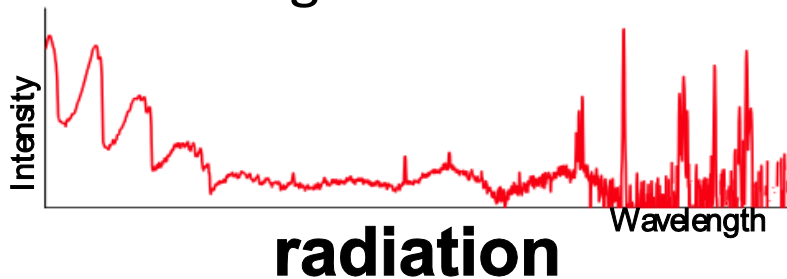
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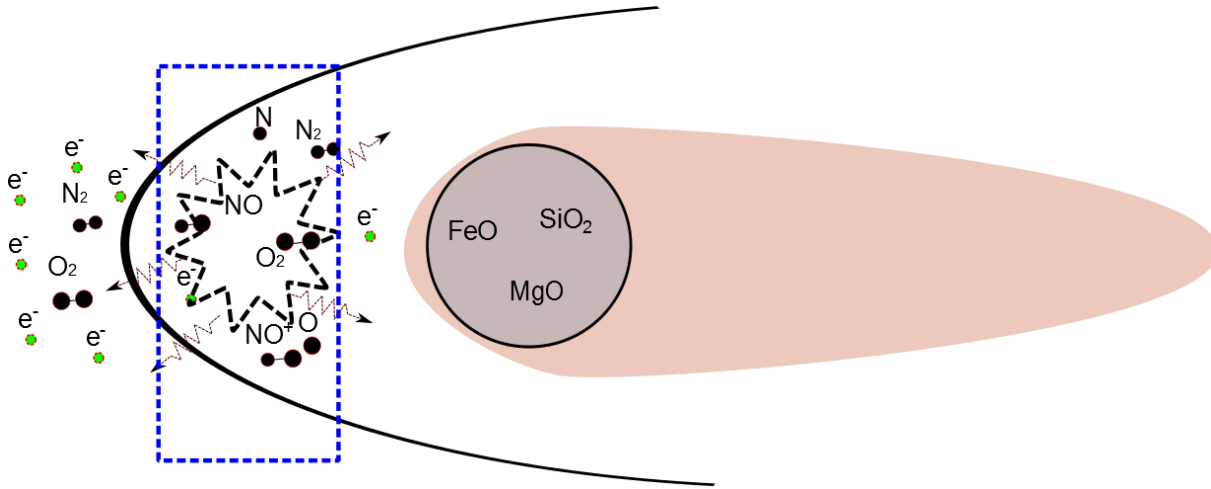
# Flow field modeling



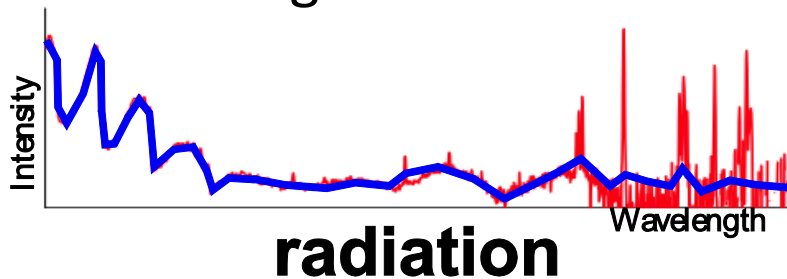
- High entry velocity (11.2 –72.5 km/s)
- High temperatures (*e.g.* 120,000 K): thermal non-equilibrium effects
- Complex chemical reactions (*e.g.* dissociation and ionization)
- High radiative field: computational expensive



# Flow field modeling



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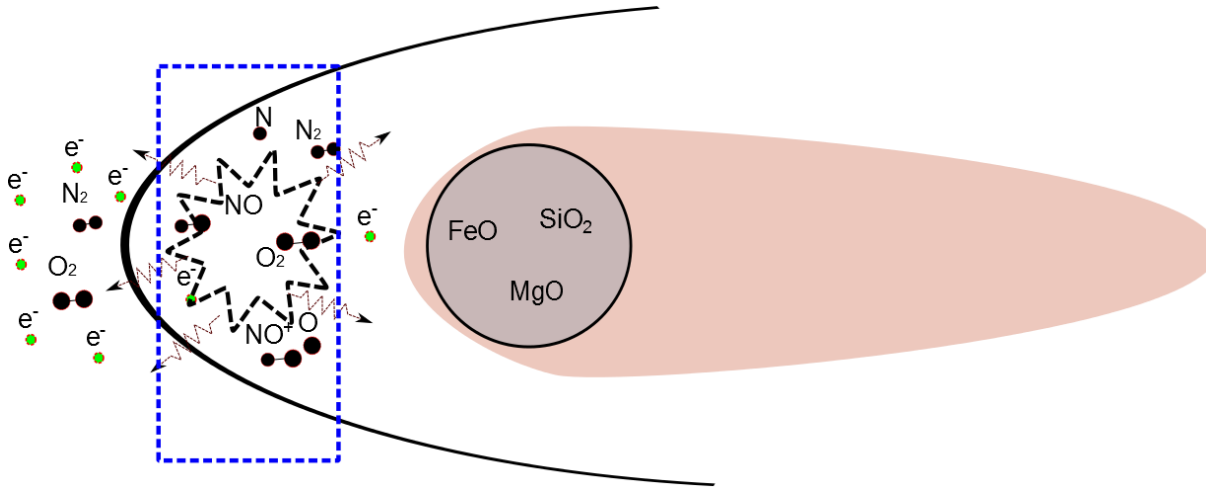


## Hybrid Statistical Narrow Band (HSNB) method<sup>1</sup>

- Accurate description
- Low CPU cost for coupling
- Atomic line treated by Line-by-Line method

<sup>1</sup> Soucasse *et al*, JQSRT (2016)

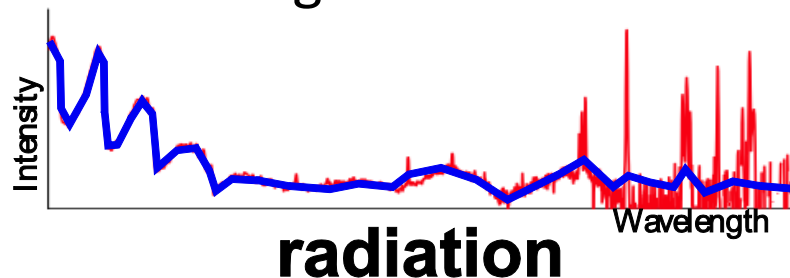
# Flow field modeling



## Assumptions:

- Atmospheric Gas reactions: non equilibrium
- Ablations products: frozen
- Only air radiation mechanisms considered

- High entry velocity (11.2 –72.5 km/s)
- High temperatures (*e.g.* 120,000 K): thermal non-equilibrium effects
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## Hybrid Statistical Narrow Band (HSNB) method<sup>1</sup>

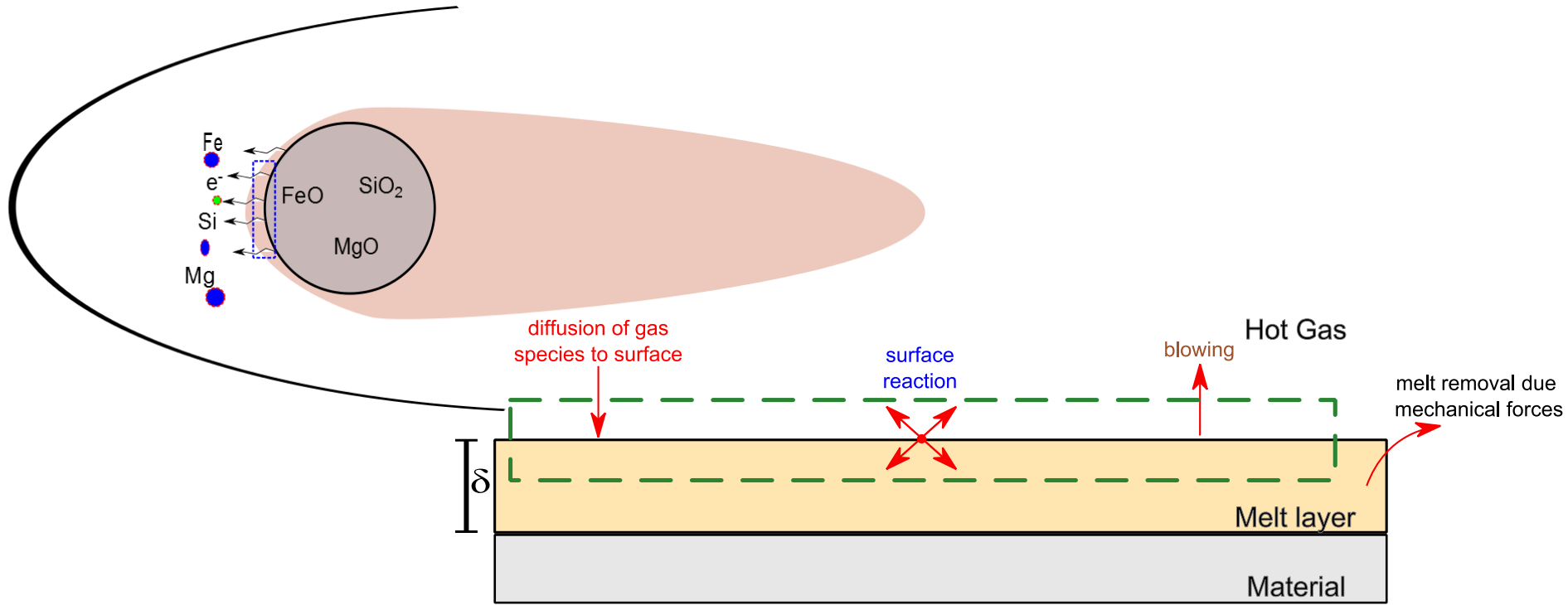
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# Ablation Model Surface Mass Balance (SMB)



Mass removal due to evaporation :

- Species  $i$  mass balance (  $O_2, N_2, \dots, FeO, Fe, SiO_2, MgO, \dots$ ):

$$J_{i,w} + \sum_{r=1}^{N_r} \omega_i^r = (\rho u)_w y_{i,w} \quad i=1, \dots, N_s \quad (1)$$

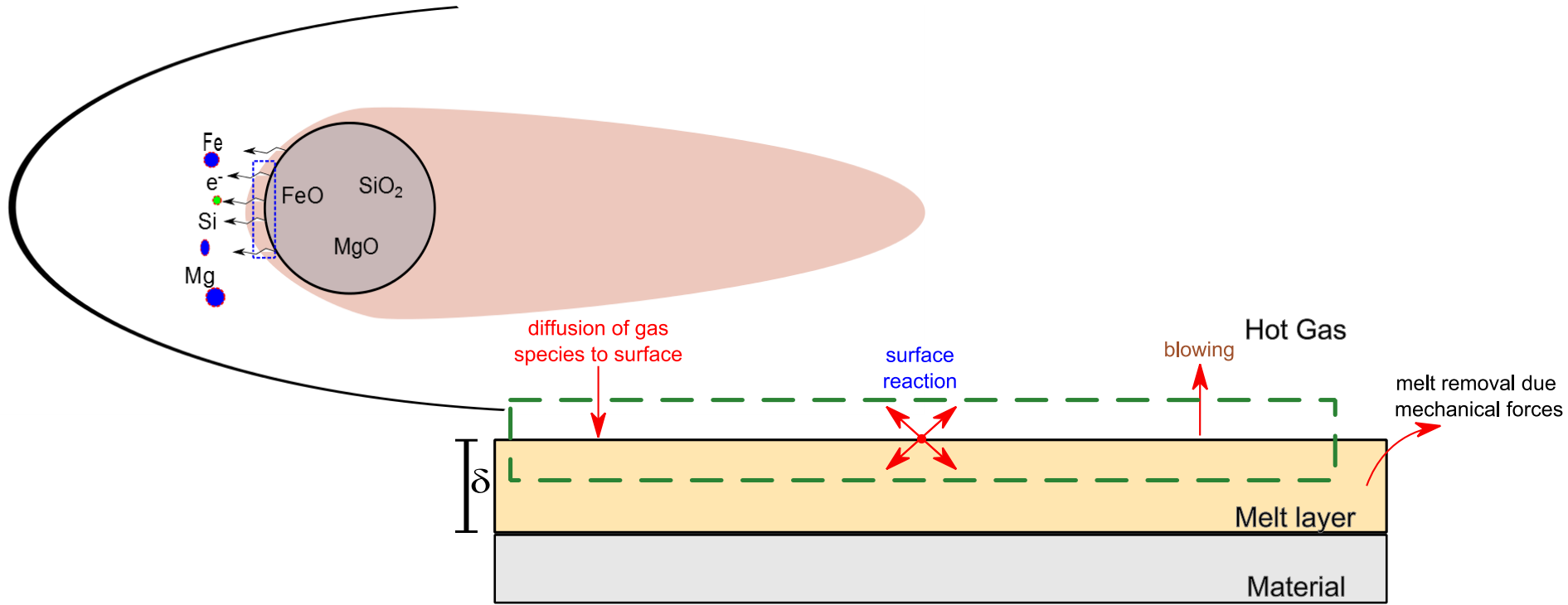
Mass removal due to mechanical forces :

- Tangential velocity<sup>1</sup>:

$$v = \tau_{flow/melt} \int_0^{\delta} \frac{dr}{\mu(T)} + \frac{1}{R} \frac{\partial P}{\partial \theta} \int_{flow/melt}^{\delta} \frac{r}{\mu(T)} dr$$

<sup>1</sup> *Bethe et al*, Journal of the Aerospace Sciences Vol.26, No.6 (1959)

# Ablation Model Surface Mass Balance (SMB)



Mass removal due to evaporation :

- **Elements**  $k$  mass balance ( O, N, ..., Fe, Si, Mg, ...):

$$\sum_{i=1}^{N_s} \sigma_{i,k} \frac{M_k}{M_i} (1) \Rightarrow J_{i,k} + \dot{m}_{evap} y_{k,s} = (\rho u)_w y_{k,w} \quad k=1, \dots, \epsilon$$

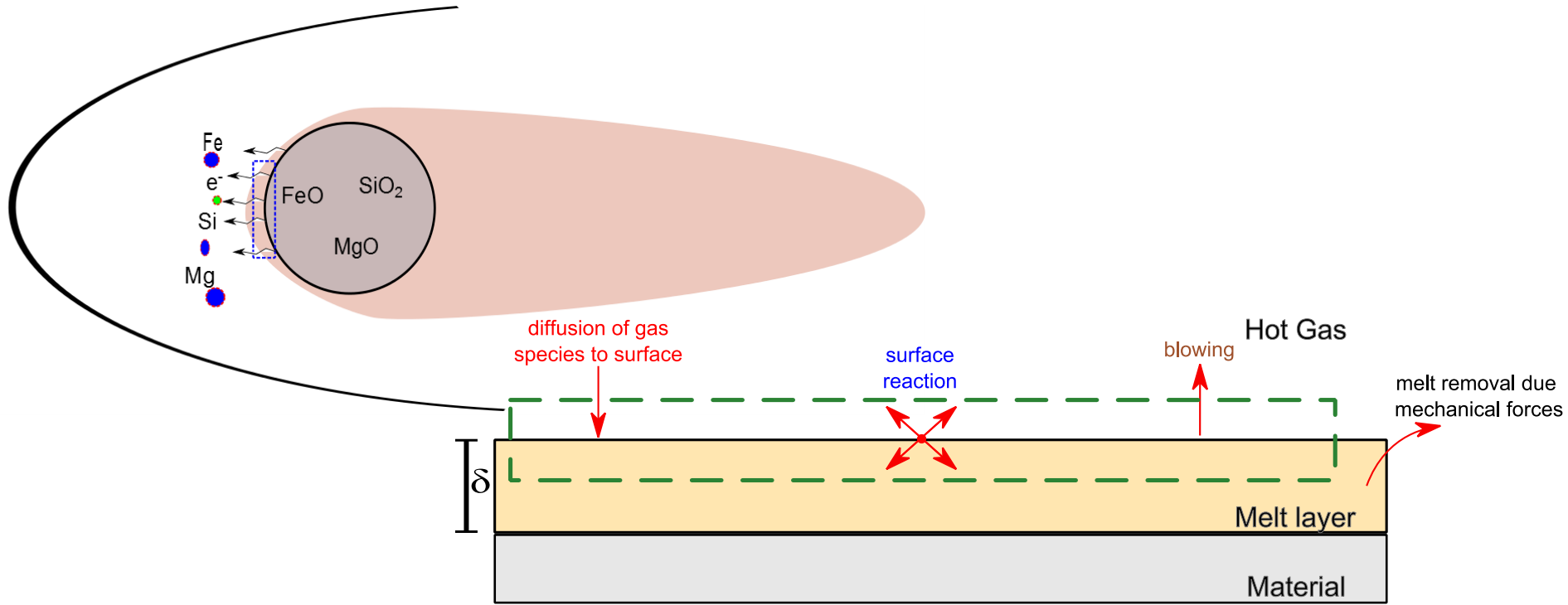
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# Ablation Model Surface Mass Balance (SMB)



## Total mass removal

Mass removal due to evaporation :

Mass removal due to mechanical forces :

- evaporation mass blowing rate,  $\dot{m}$ :

$$\dot{m}_{evap} = \frac{J_{i,k}}{(y_{k,w} - y_{k,s})}$$

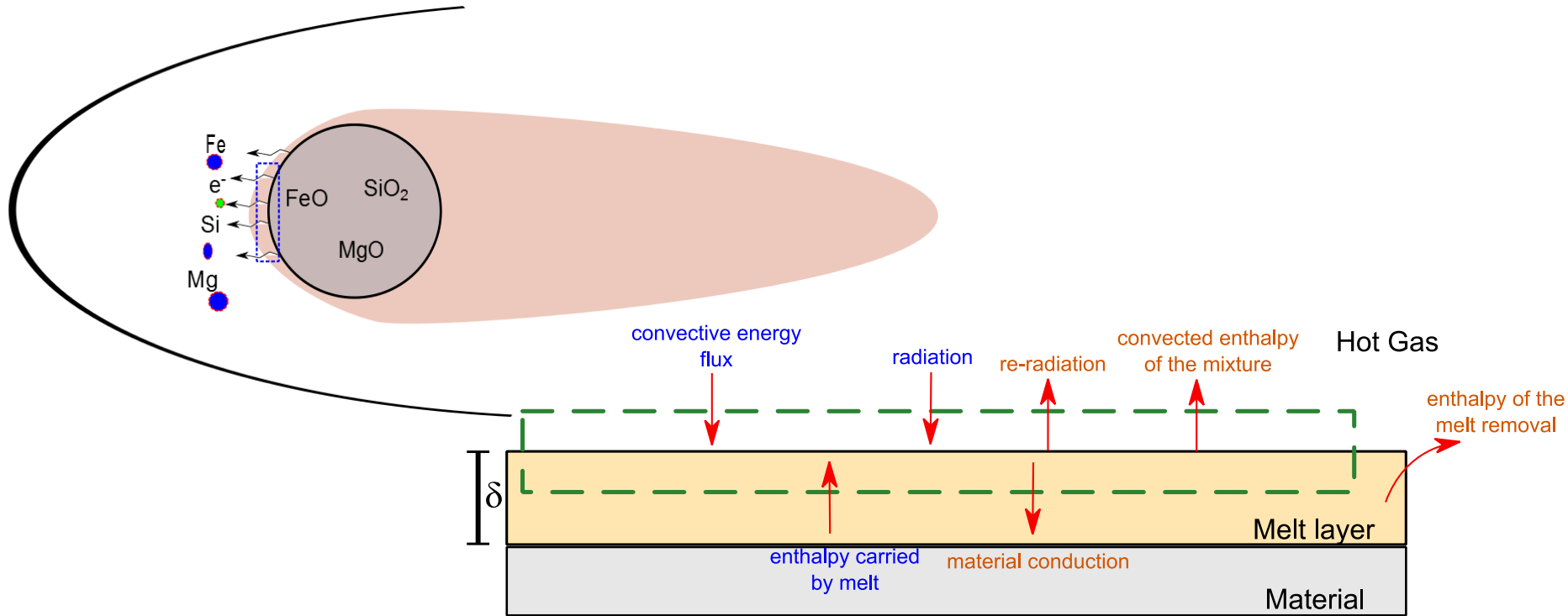
+

- mass removal :

$$\dot{m}_{melt} = \rho_{melt} v$$

- $y_{k,w}$  : gaseous mixture at the wall computed by chemical equilibrium
- $J_{i,k}$  : elemental mass diffusion computed by CFD

# Ablation Model Surface Energy Balance (SEB)



- Energy Balance:

$$q_{convective} + (\dot{m}_{evap} + \dot{m}_{melt})h_c + q_{rad,in} = q_{rad,out} + \dot{m}_{evap}h_w + k \frac{\partial T}{\partial r} + \dot{m}_{melt}h_c$$

# A surface composed by multiple constituents

Classification	Composition	Elemental composition
Simplify Ordinary Chondrite	SiO <sub>2</sub> : 0.606	Si: 0.232
	MgO: 0.394	Mg: 0.152
		O: 0.616

Meteor surface properties

How to compute  $y_{k,w}$  for a multi element surface?<sup>1</sup>

## Multiphase Equilibrium solver<sup>2</sup>

- Multiphase Gibbs function continuation (MPGFC)<sup>3</sup>
- Impose any linear constraint to the system:

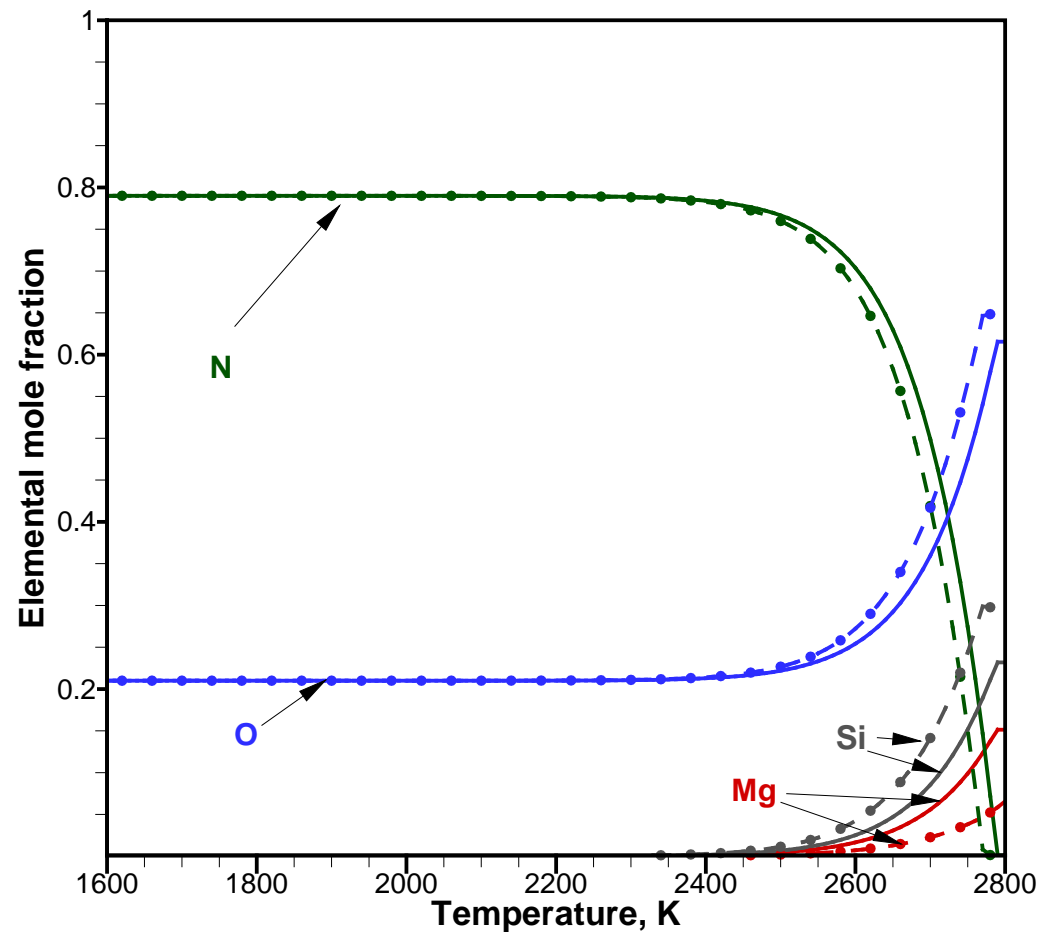
$$\frac{x_{Si}}{x_{Mg}} = const$$

<sup>1</sup> First addressed by *Milos et al*, AIAA 97-0141 (1997)

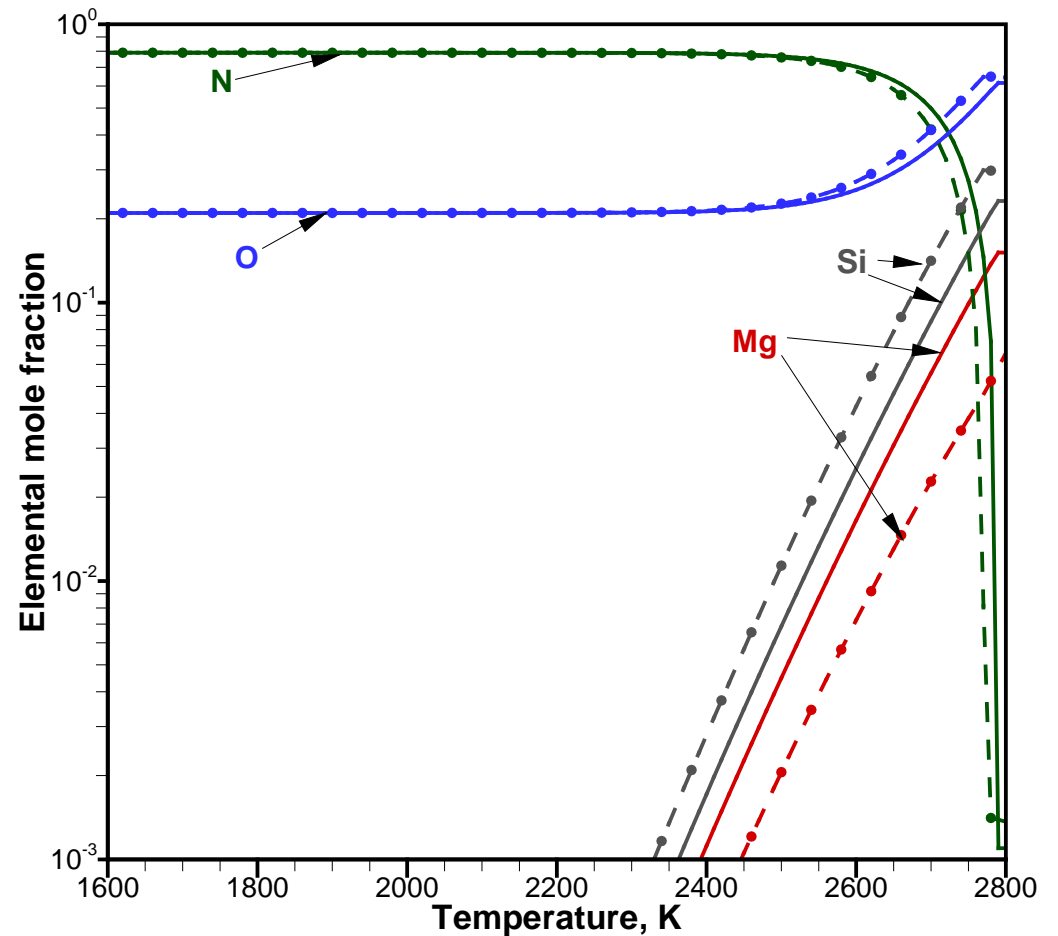
<sup>2</sup> Developed by *Scoggins et al*, Combust. Flame 2015

<sup>3</sup> Extension Gibbs Function Continuation(GFC) by *Pope et al*, FDA 03-02 (2003)

# Multi species surface equilibrium



Constraint vs Unconstrained



Constraint vs Unconstrained (log scale)

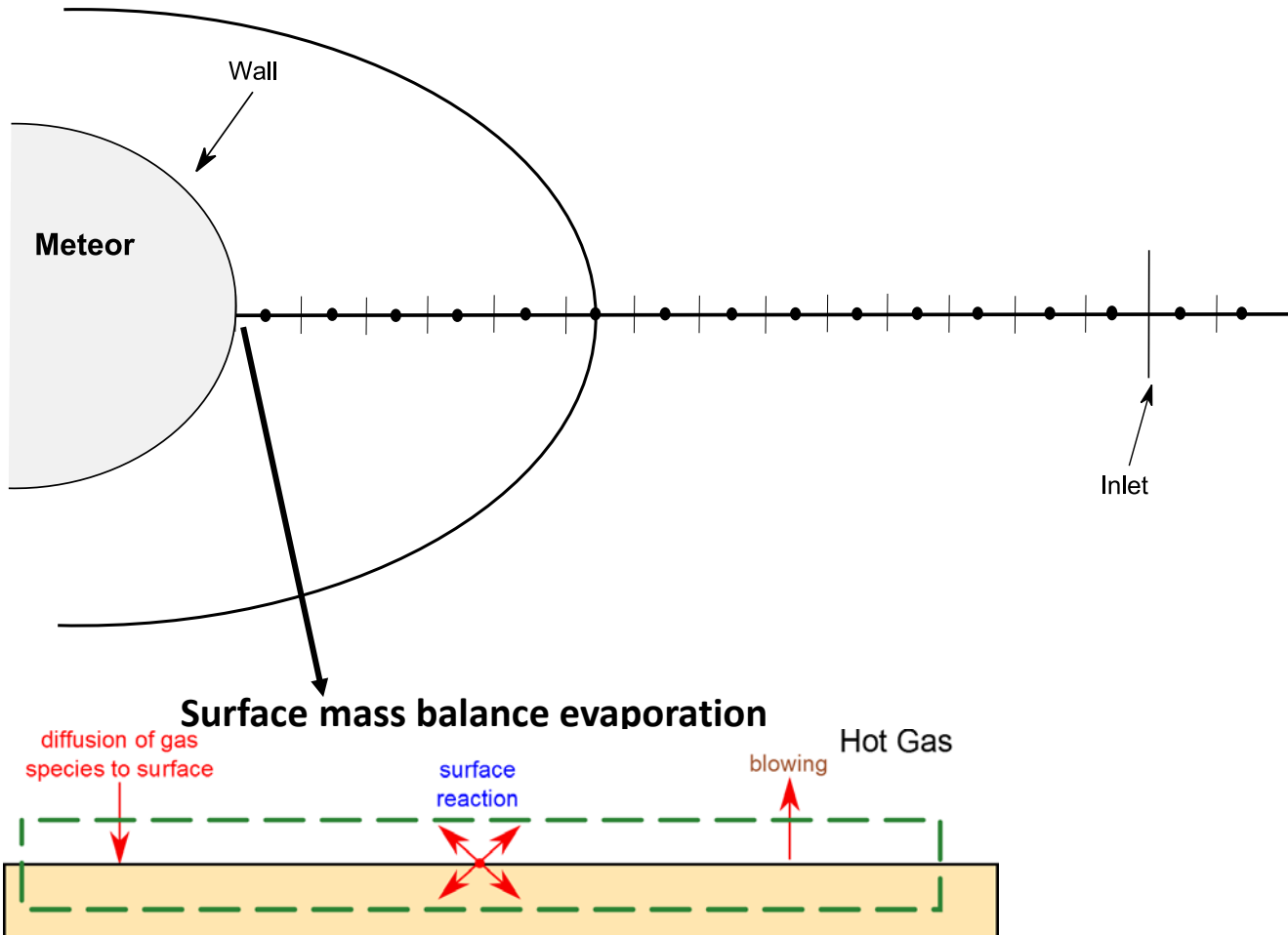
Gaseous Elemental mole fraction vs Temperature, 0.09 atm;

— constrained, -•- unconstrained equilibrium

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# Meteor ablation flow solver



## Stagnation-Line Code CFD Solver <sup>1</sup>

- 1D Stagnation-Line solver in spherical coordinates
- Cell-centered finite volume
- Roe's Riemann solver
- Fully implicit time-integration

$$\frac{\partial}{\partial t} \mathbf{U} + \frac{\partial}{\partial r} \mathbf{F}^{\text{inv}} + \frac{\partial}{\partial r} \mathbf{F}^{\text{vis}} + \frac{\mathbf{G}^{\text{inv}} + \mathbf{G}^{\text{vis}}}{r} = \mathbf{S}$$

coupled

## Mutation<sup>++</sup> library <sup>2</sup>

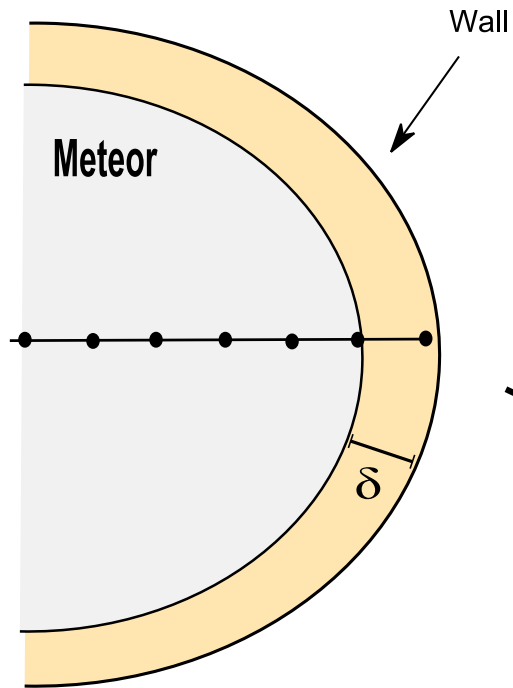
- Thermodynamic properties
- Transport properties
- Air chemistry
- Multiphase Equilibrium Solver<sup>3</sup>

<sup>1</sup> Munafò et al, Phys. Fluids 26, 097102 (2014)

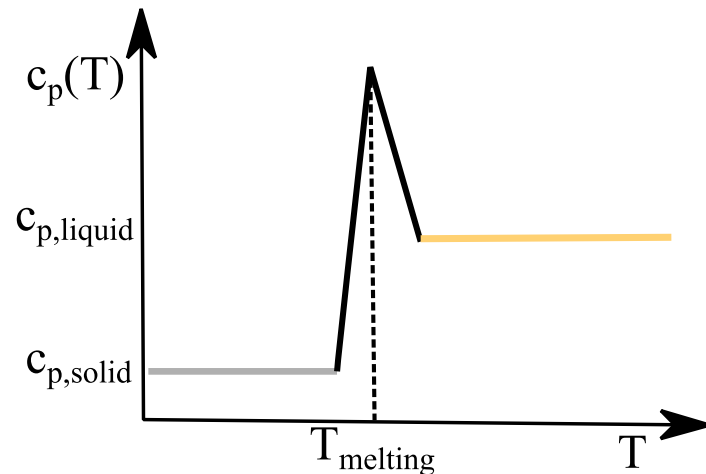
<sup>2</sup> Scoggins et al, AIAA 2014-2966 (2014)

<sup>3</sup> Scoggins et al, Combust. Flame 162(12):4514-4522 (2015)

# Meteor ablation material solver



Variable thermodynamic properties:

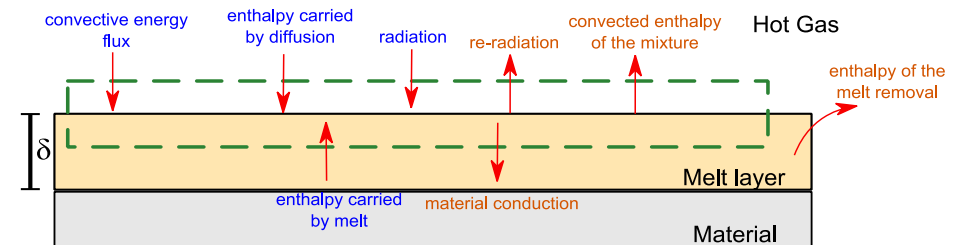


## Melting material solver

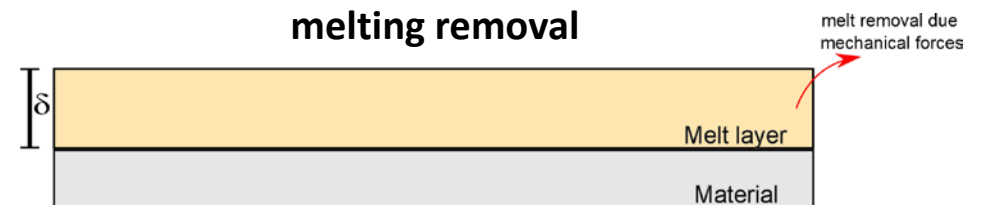
- 1D in spherical coordinates
- Finite difference method
- Unsteady solver
- Explicit time integration

$$\rho c_p(T) \frac{\partial T}{\partial t} = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 k \frac{\partial T}{\partial r} \right)$$

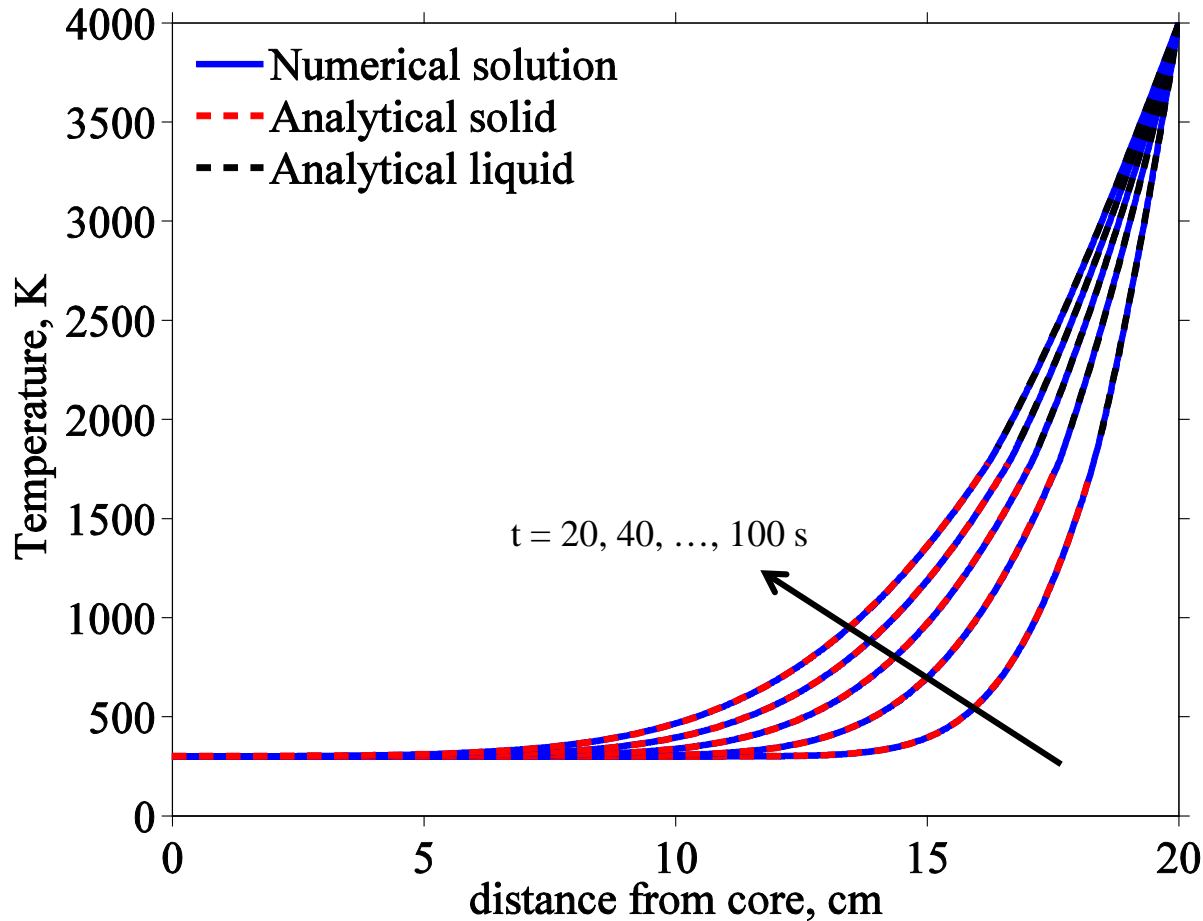
## Surface energy balance



## melting removal



# Comparisson with analytical solution<sup>1</sup>



$$T_m = 1800K$$

$$T_w = 4000K$$

$$\lambda = \frac{x_{s,l}}{2\sqrt{\mu_l t}} \quad x^* = \frac{x}{2\sqrt{\mu t}} \quad \mu = \frac{k}{\rho c_p}$$

$$\left\{ \begin{array}{l} \frac{e^{-\lambda^2}}{\operatorname{erf} \lambda} - \frac{k_s}{k_l} \sqrt{\frac{\mu_l}{\mu_s}} \frac{(T_m - T_0)}{(T_w - T_m)} \frac{e^{(-\lambda^2 \mu_l / \mu_s)}}{\operatorname{erfc} \left( \lambda \sqrt{\frac{\mu_l}{\mu_s}} \right)} = \frac{\lambda L \sqrt{\pi}}{c_{p_l} (T_w - T_m)} \\ T_l = T_w - \frac{(T_w - T_m)}{\operatorname{erf}(\lambda)} \operatorname{erf} \left( x_l^* \right), \quad \lambda < x < \infty \\ T_s = T_0 + \frac{(T_m - T_0)}{\operatorname{erfc} \left( \lambda \sqrt{\frac{\mu_l}{\mu_s}} \right)} \operatorname{erfc} \left( x_s^* \right), \quad 0 < x < \lambda \end{array} \right.$$

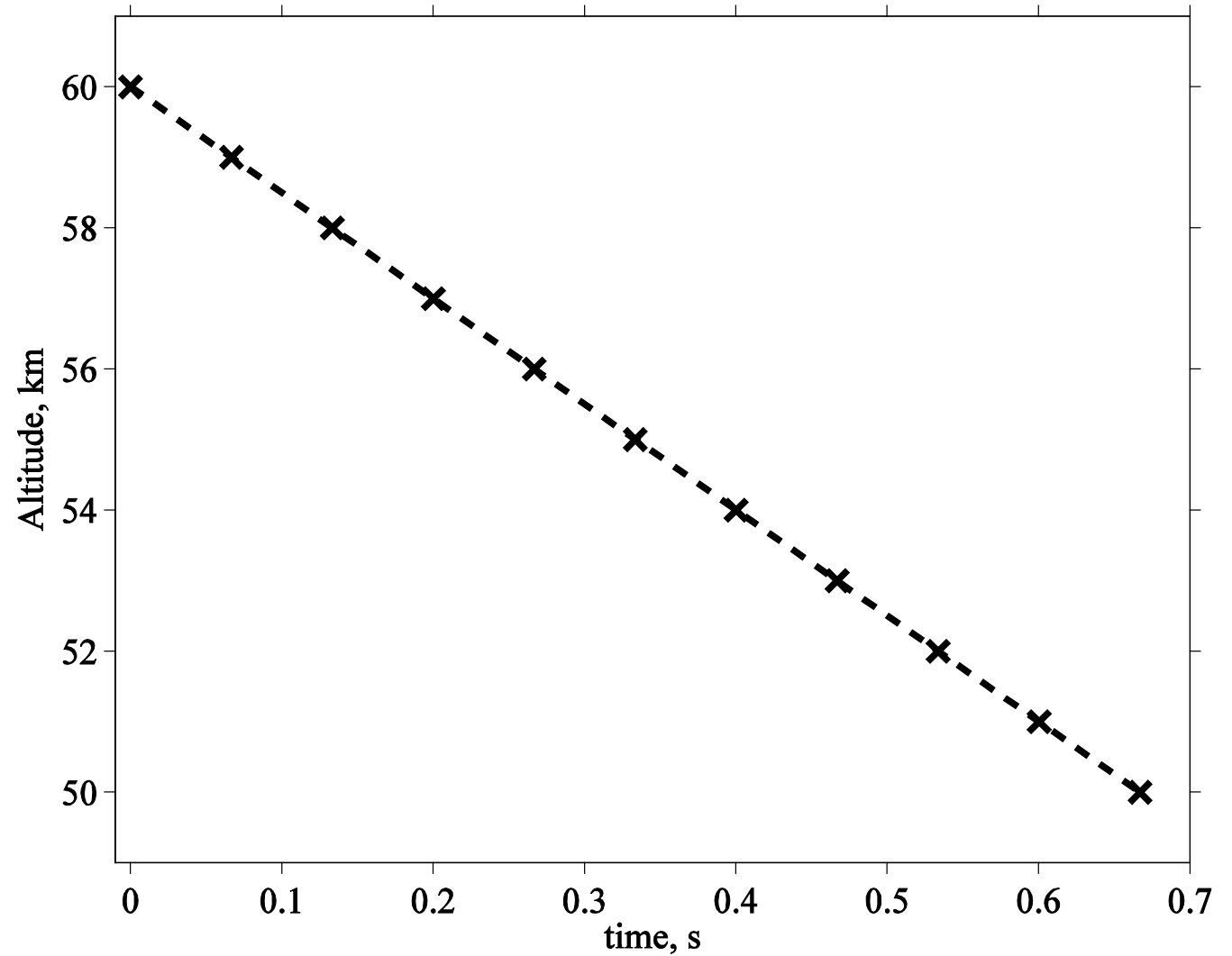
<sup>1</sup> Carslaw, H. S., and J. C. Jaeger. 1959. *Conduction of heat in solids*. Oxford: Clarendon Press.



# Flow/ material solver coupling strategy

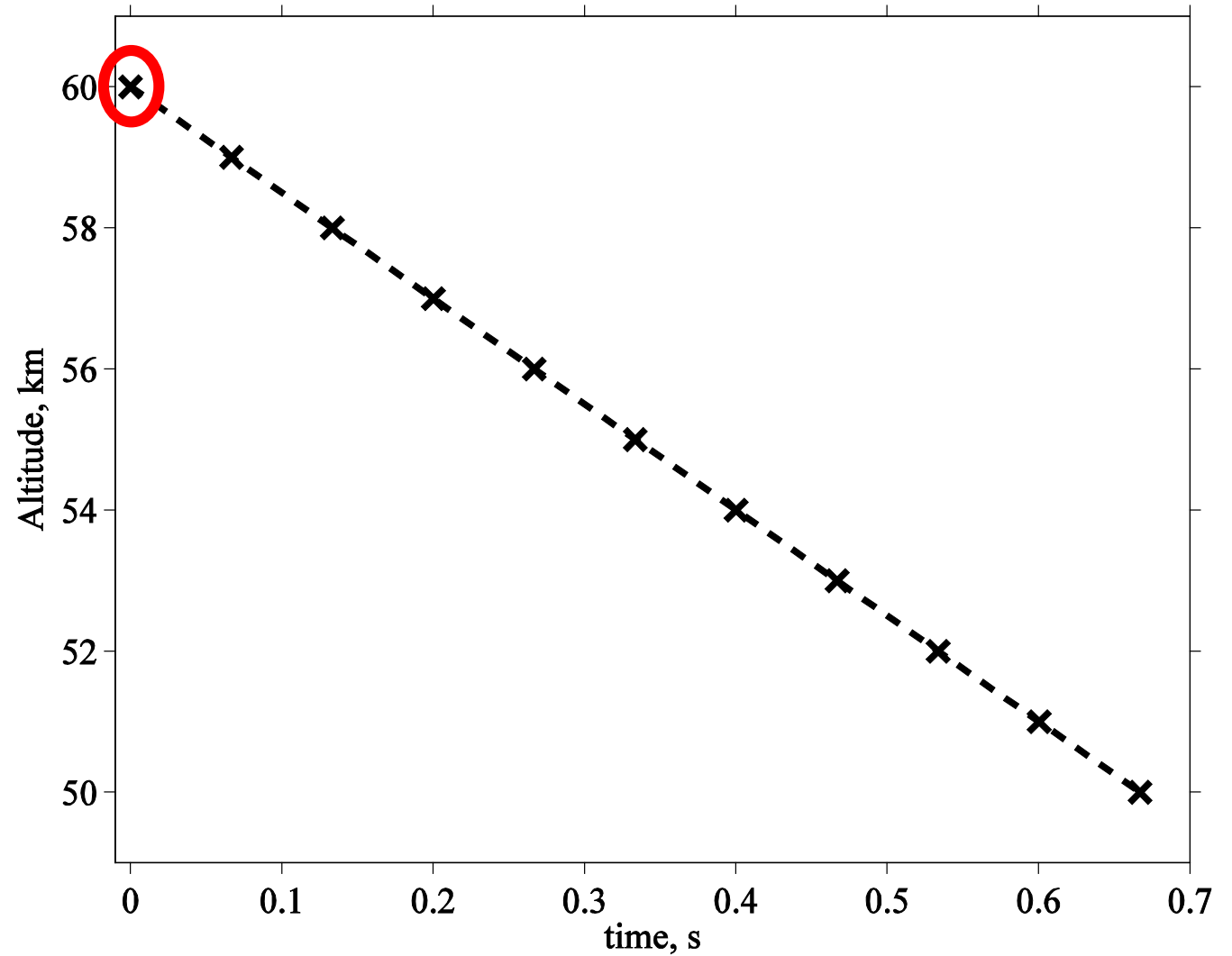
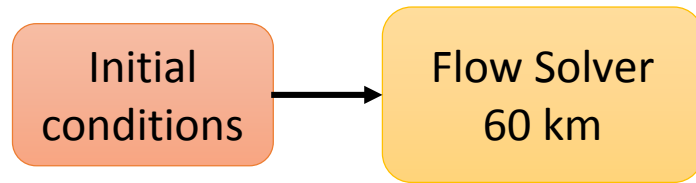
## Simulation conditions:

- Meteor composition in the atmosphere:
  - Simplify Ordinary Chondrite  
(SiO<sub>2</sub>: 0.65, MgO: 0.35) meteor, 1 cm radius
- Entry velocity: 15 km/s



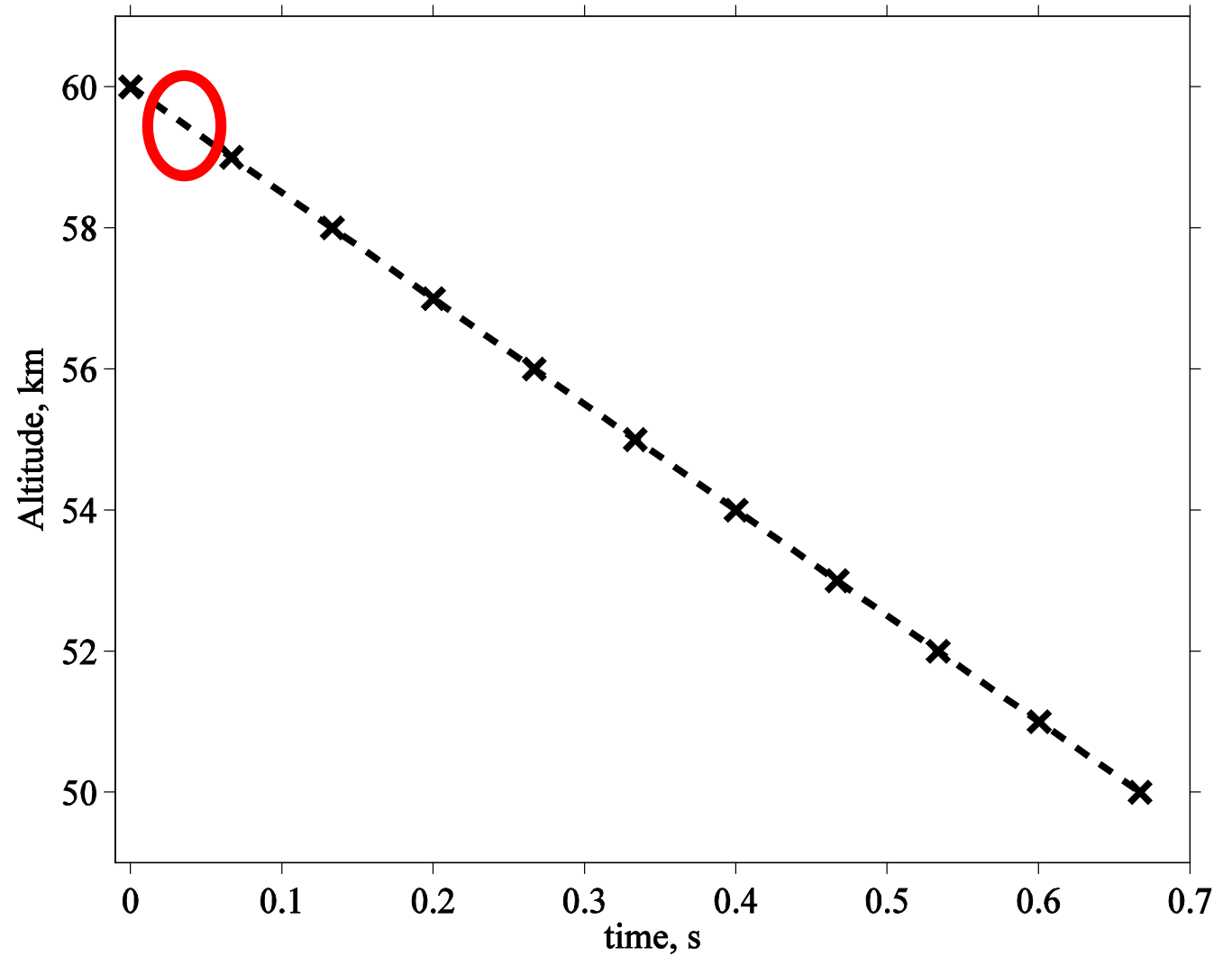
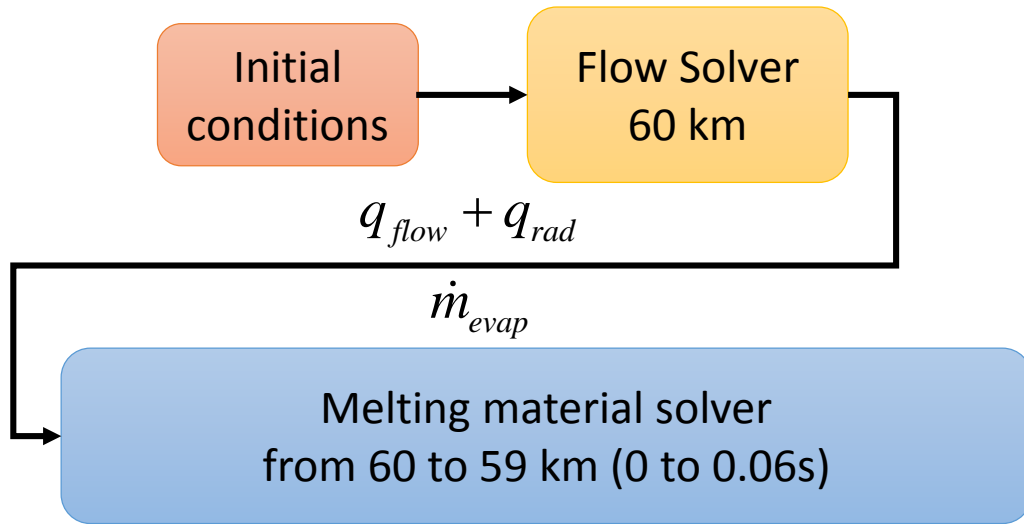
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Implicit coupling approach:



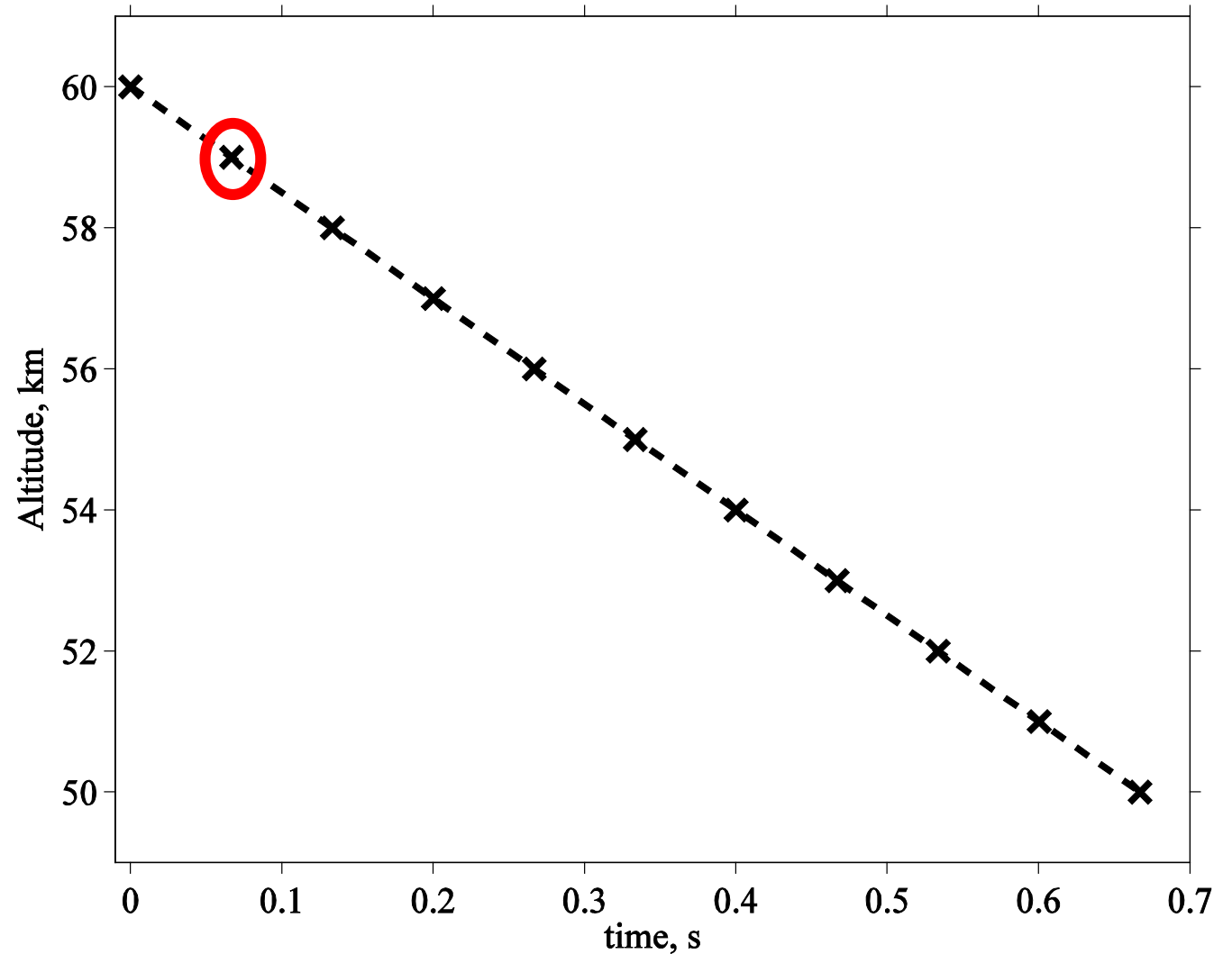
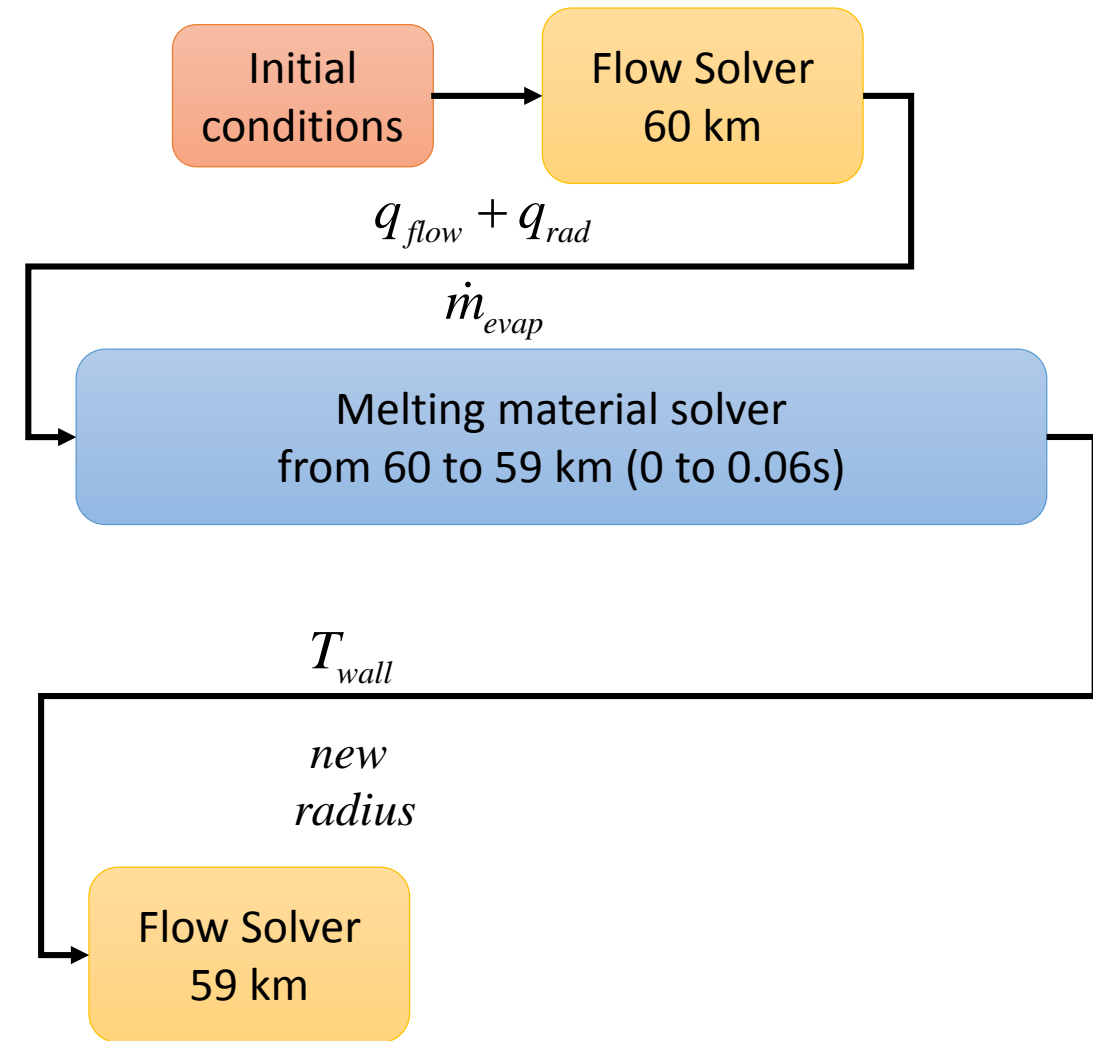
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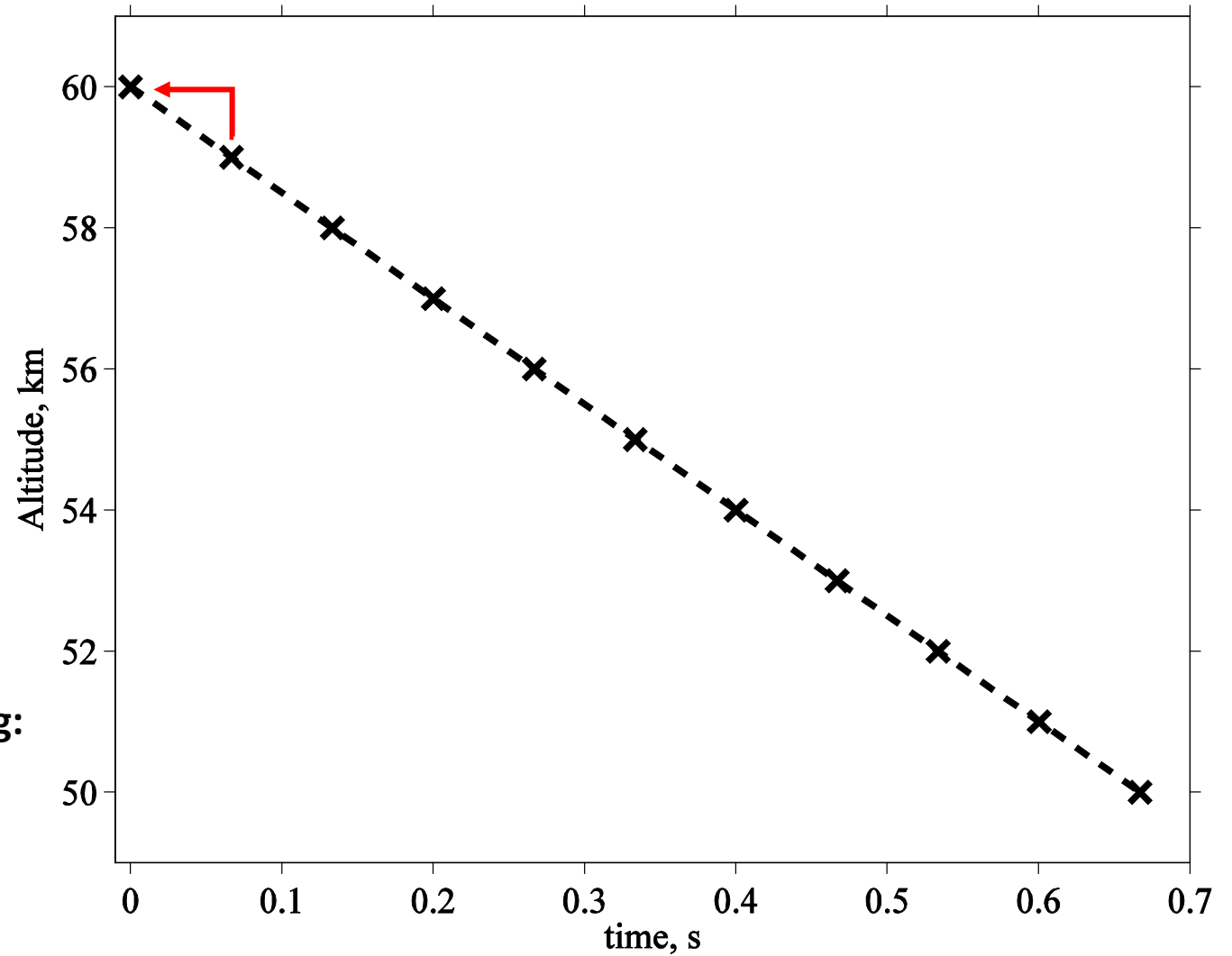
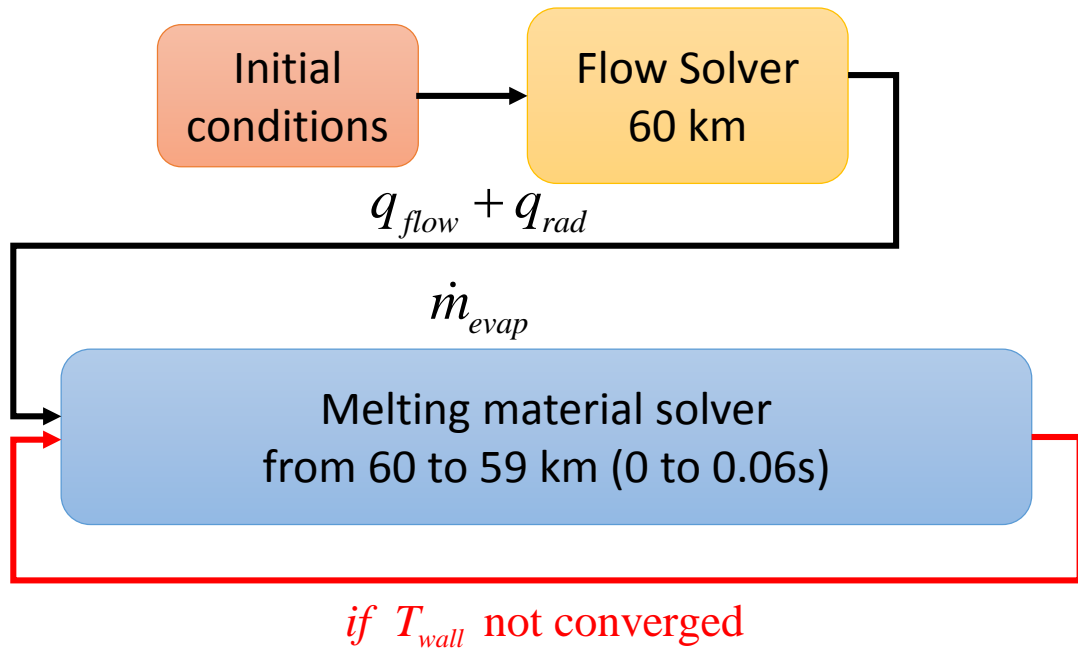
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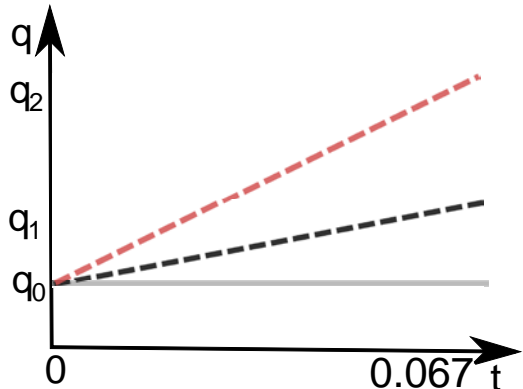


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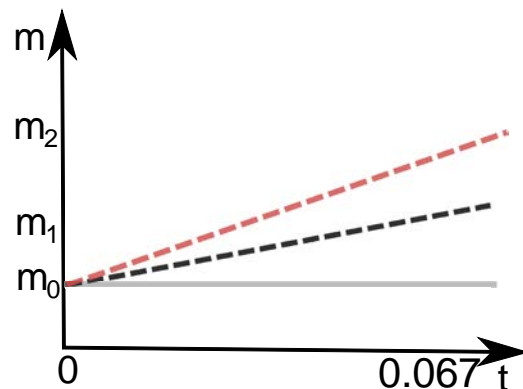
Implicit coupling approach:



Heat flux ramping:

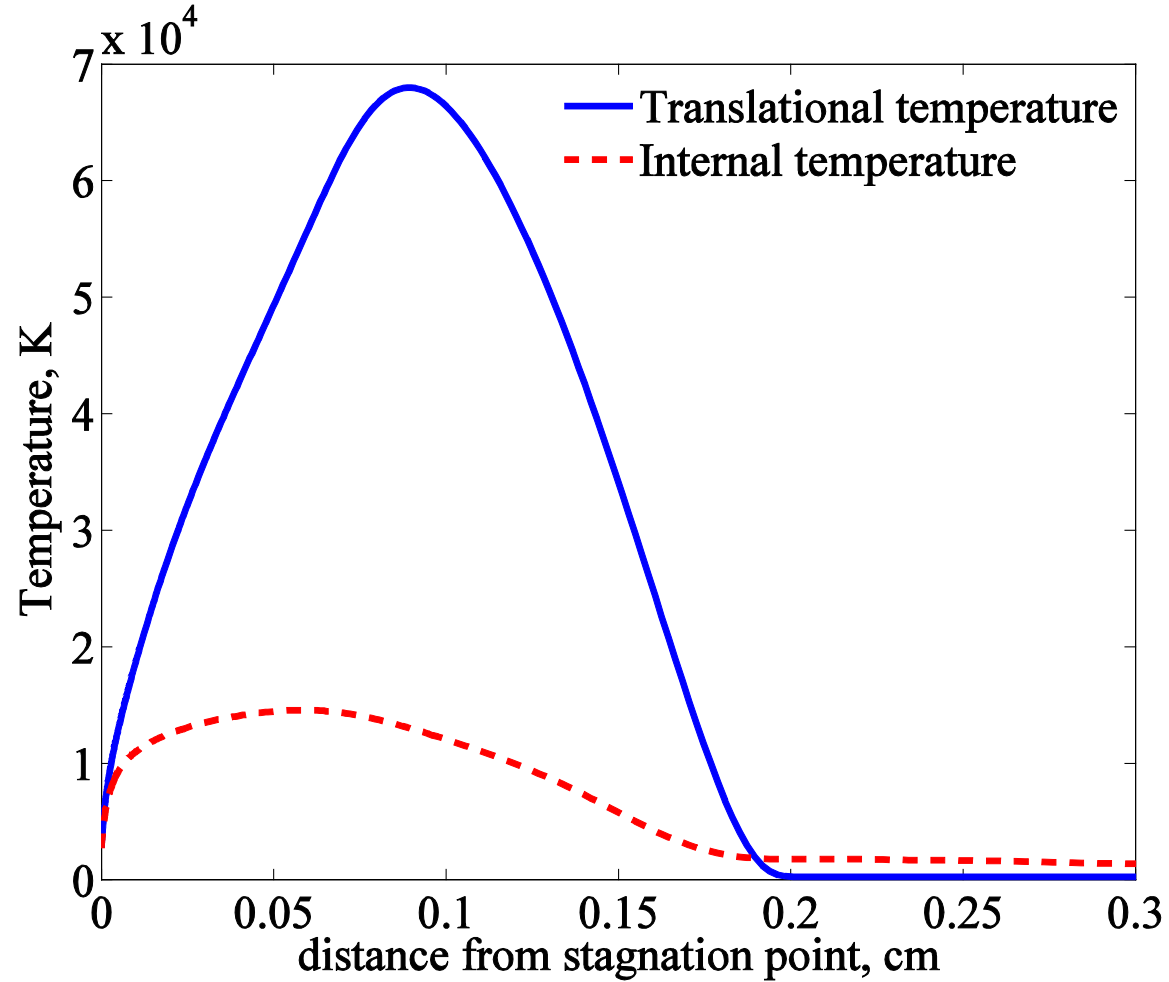


Evaporation rate ramping:

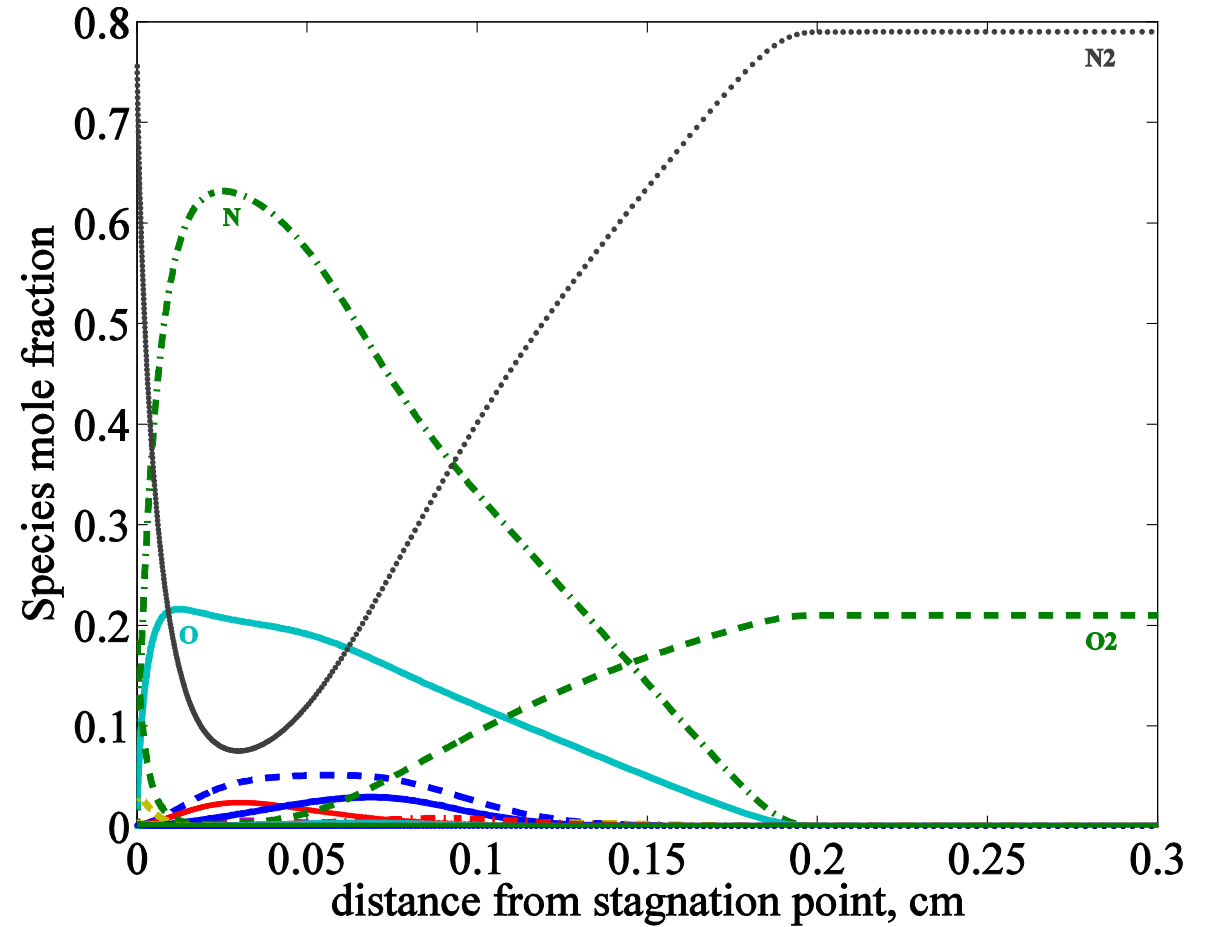


# Flow field at 60 km

Temperature along stagnation streamline

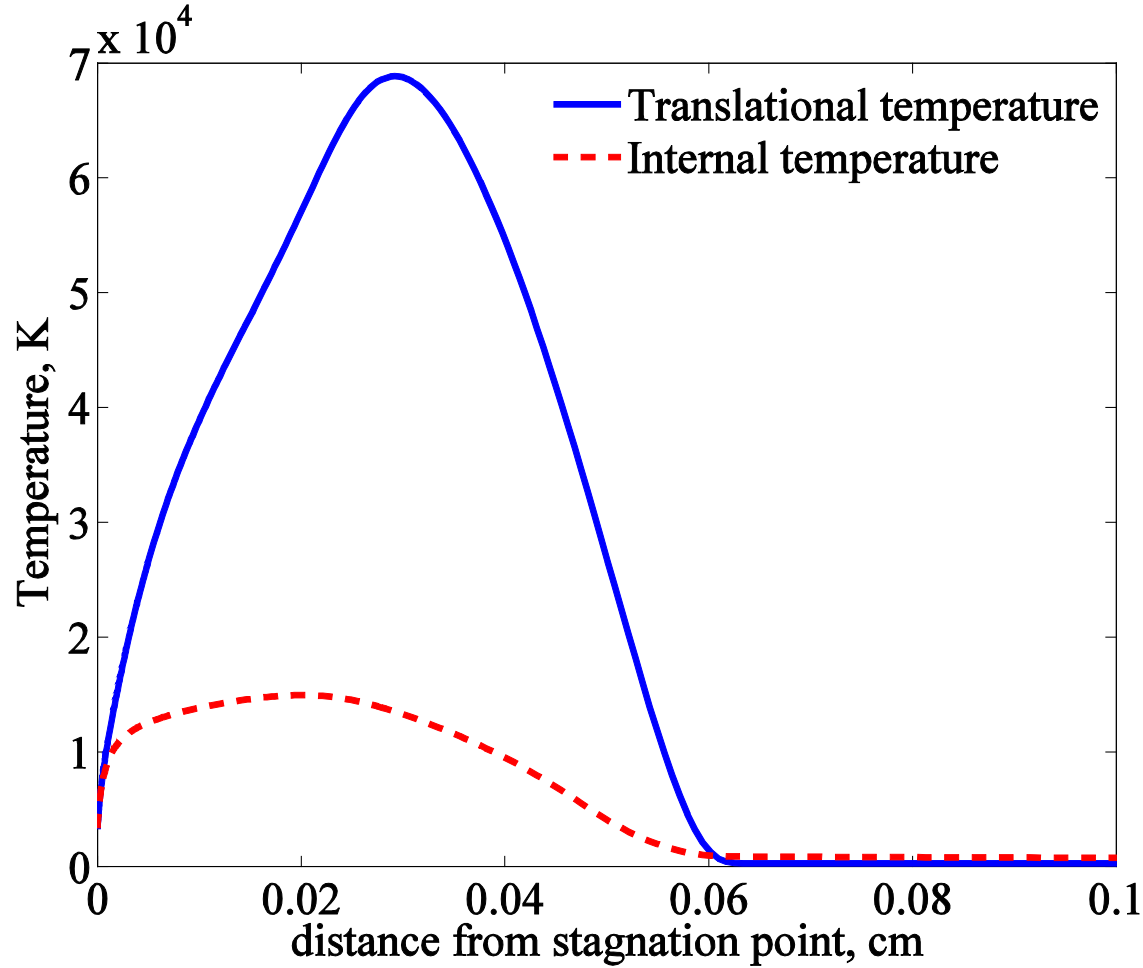


Species diffusion along stagnation streamline

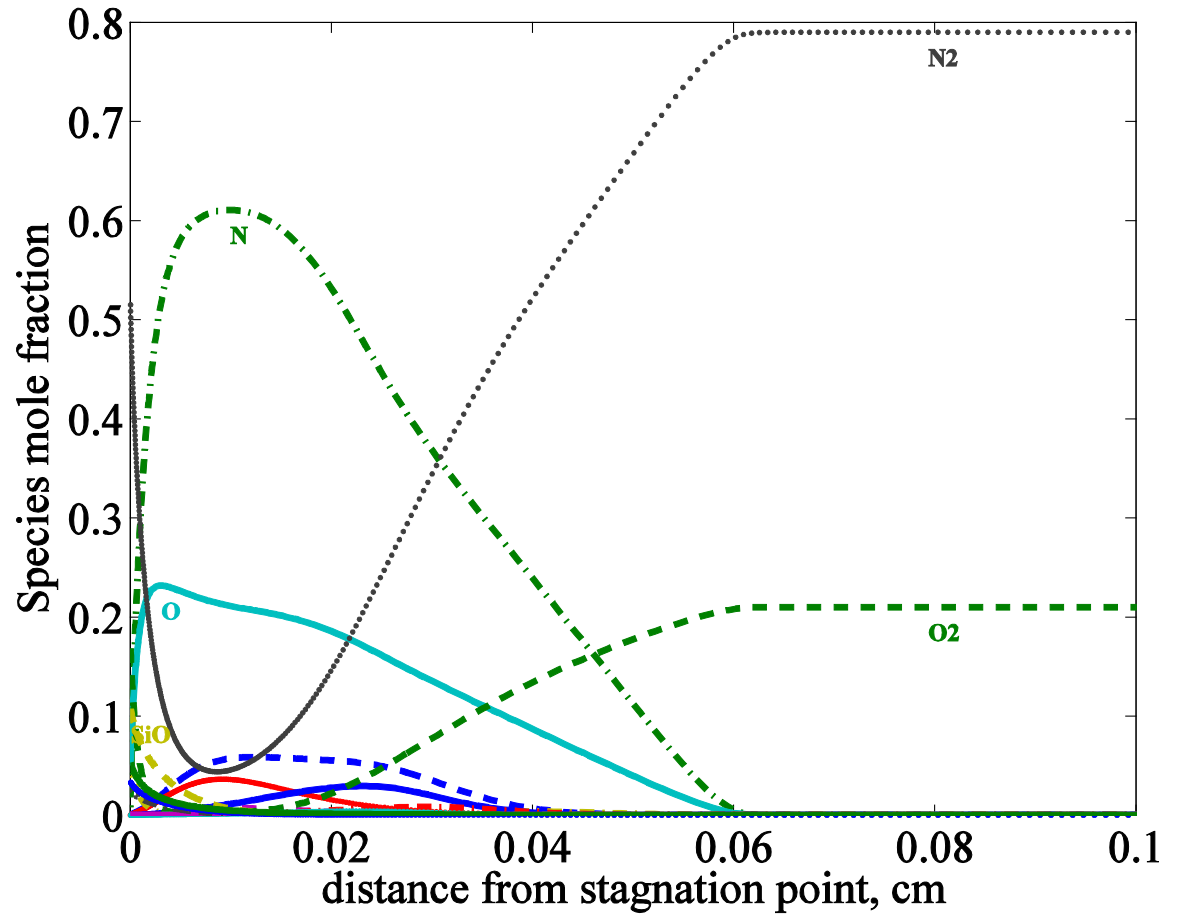


# Flow field at 50 km

Temperature along stagnation streamline

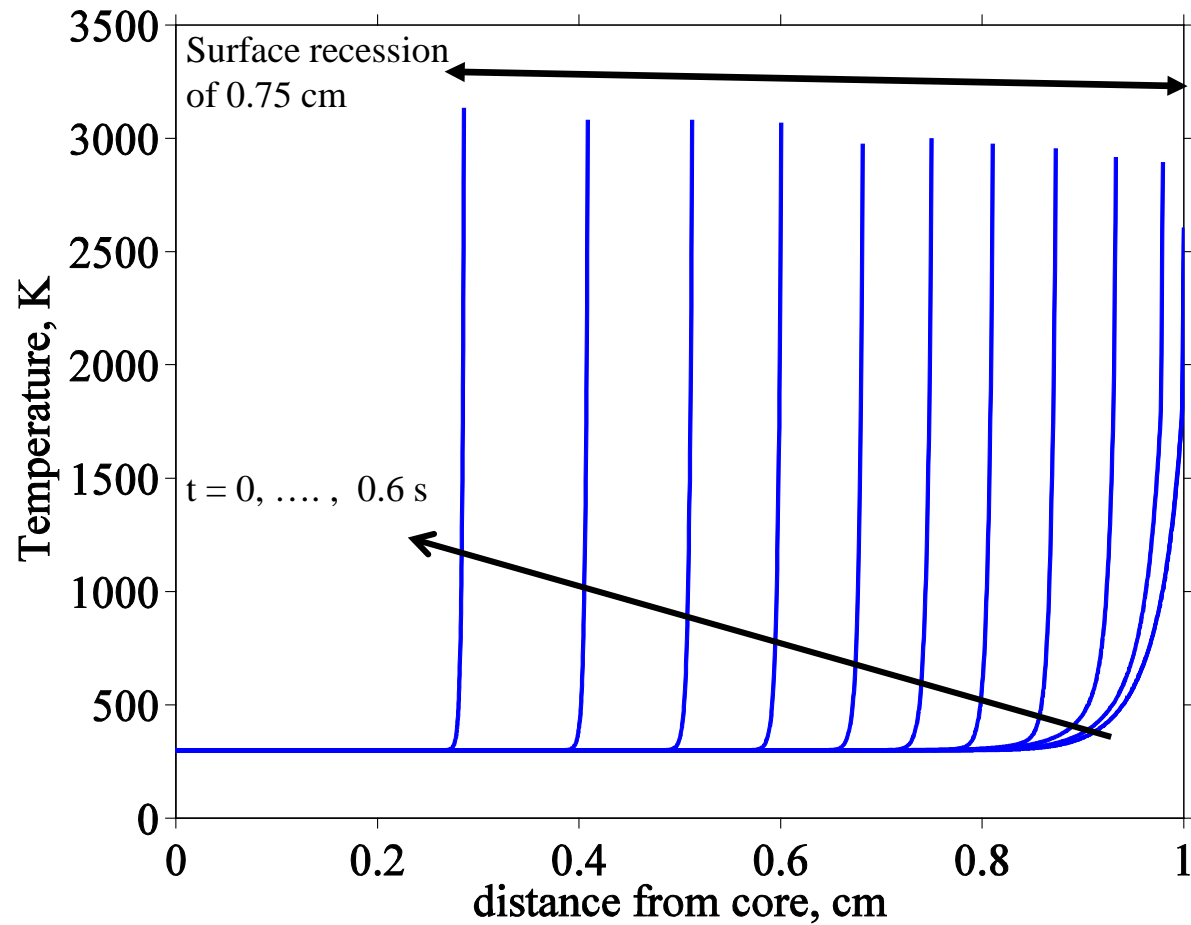


Species diffusion along stagnation streamline

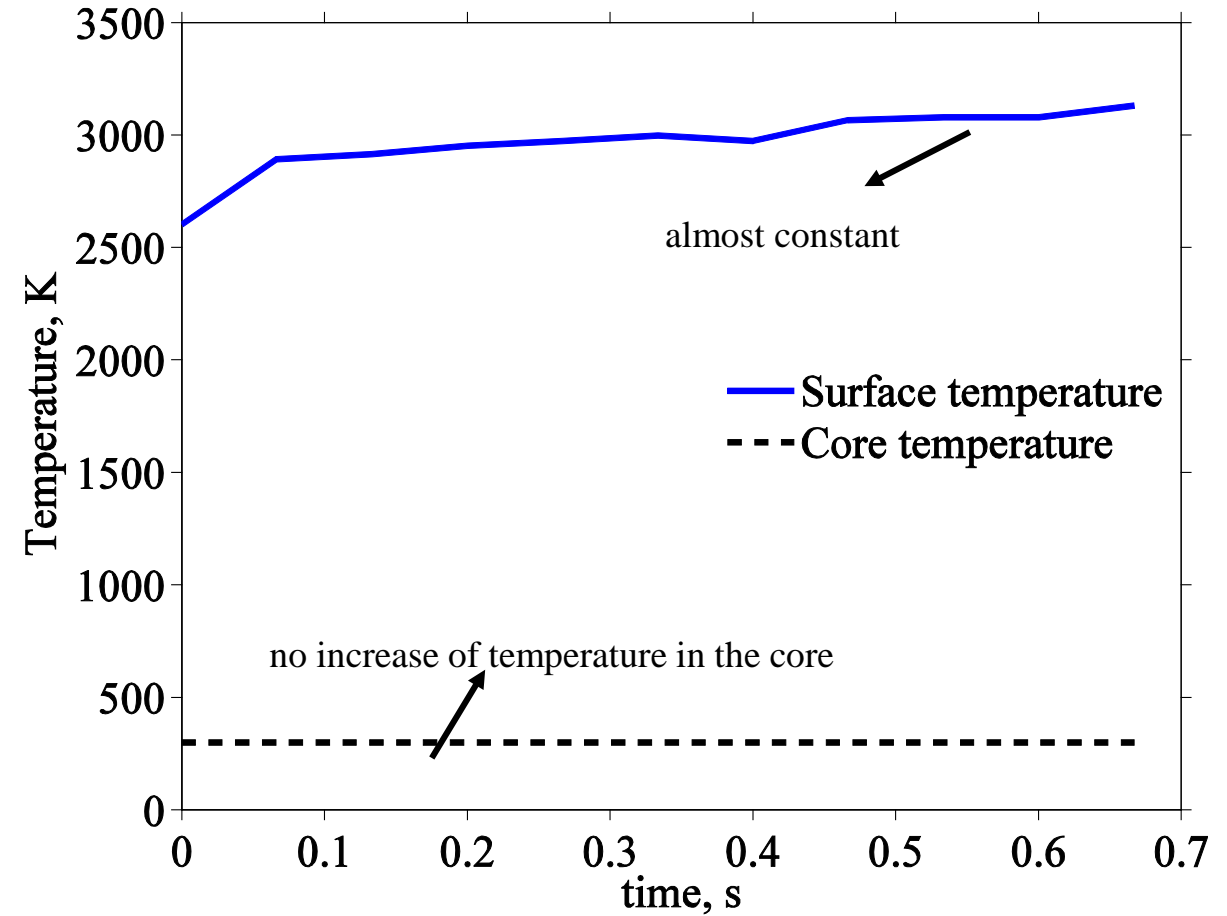


# Material response from 60 to 50 km (temperature)

Temperature distribution along the material



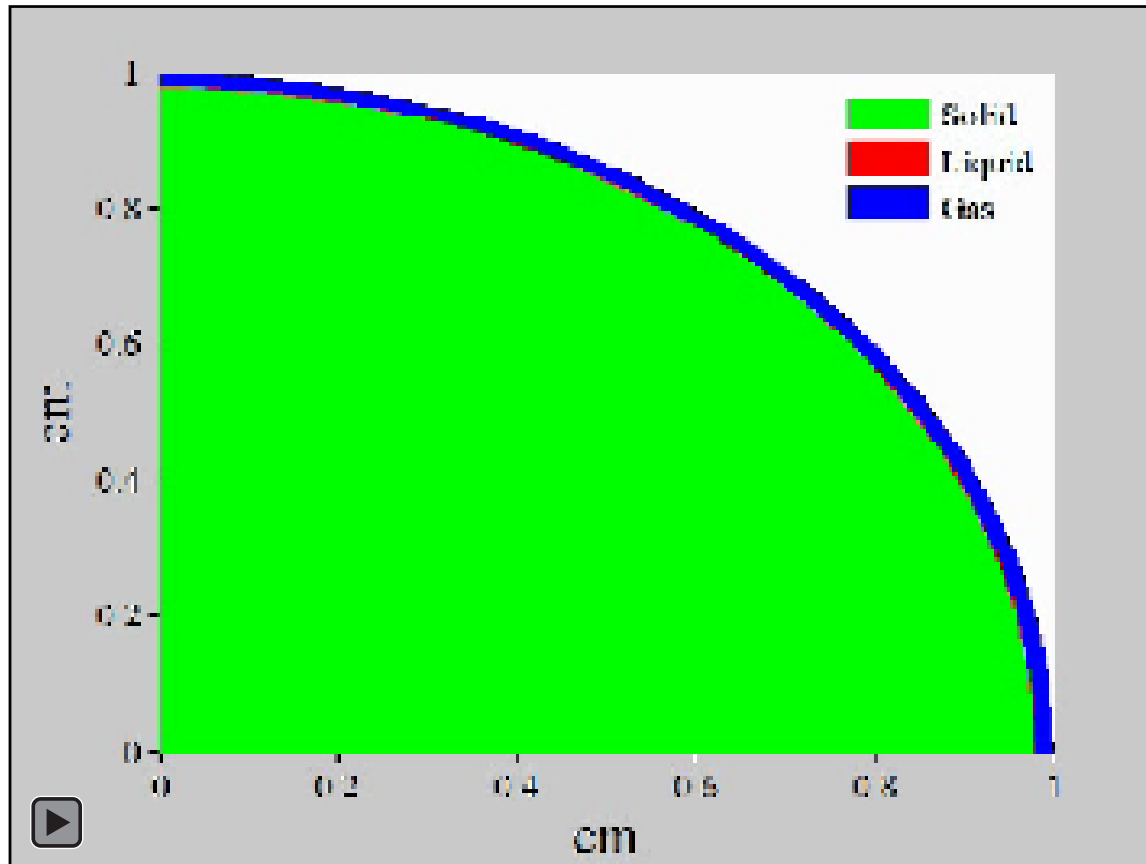
Temperature at the surface and at the core



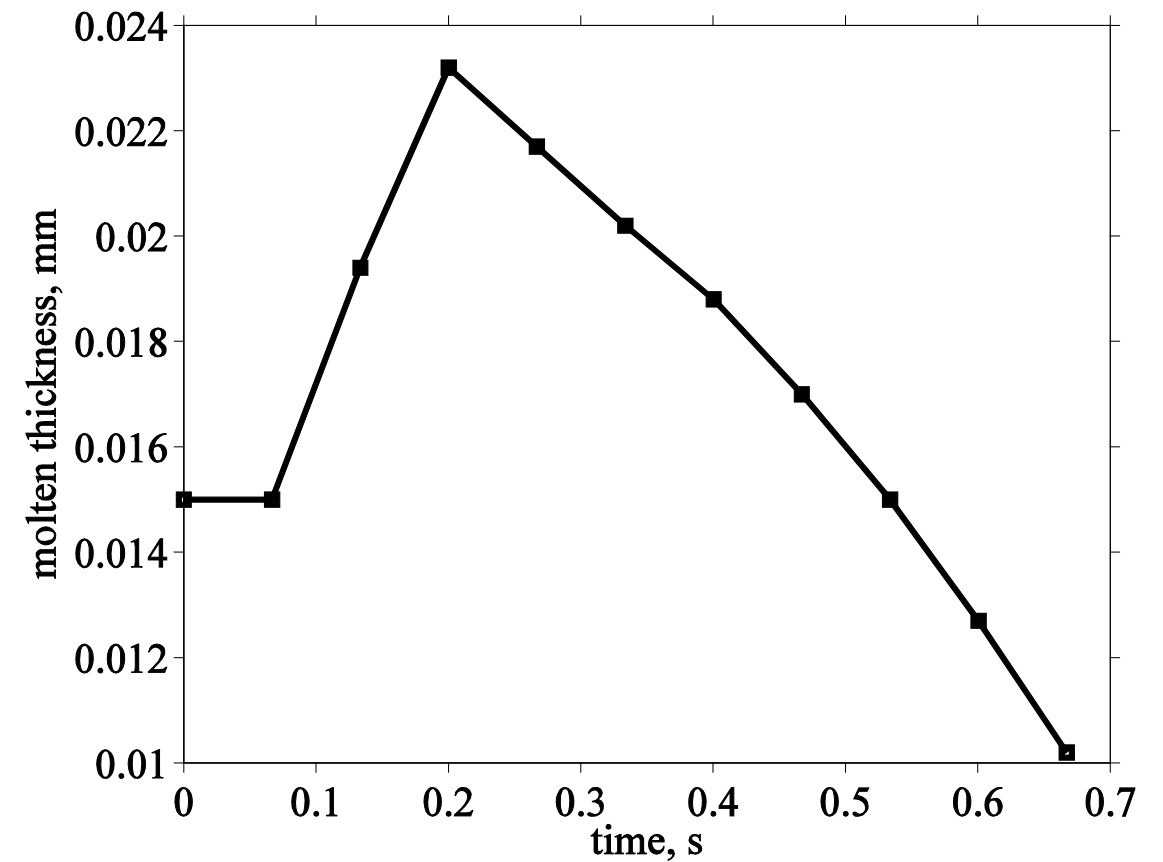


# Material response from 60 to 50 km (evaporation and melting front)

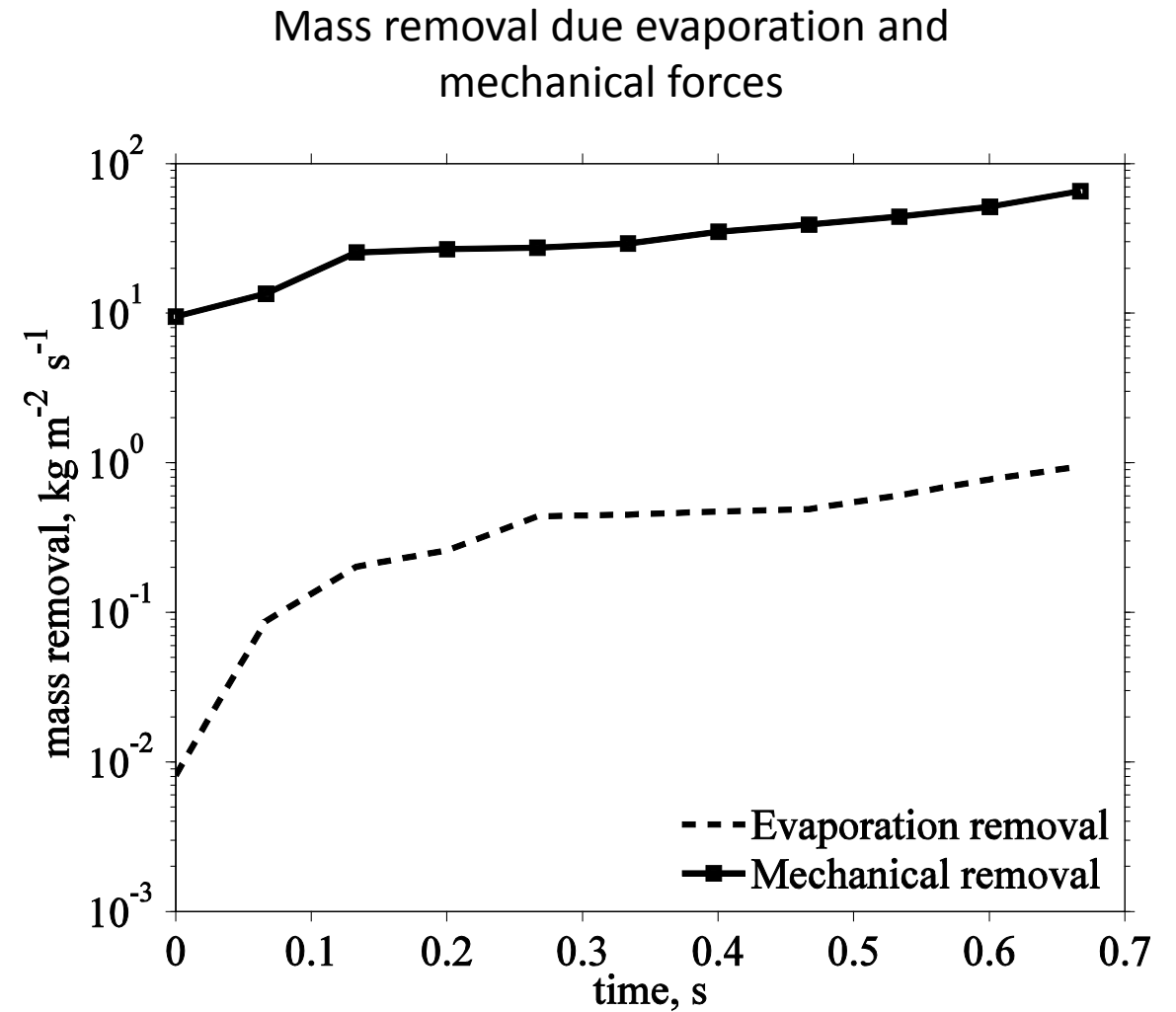
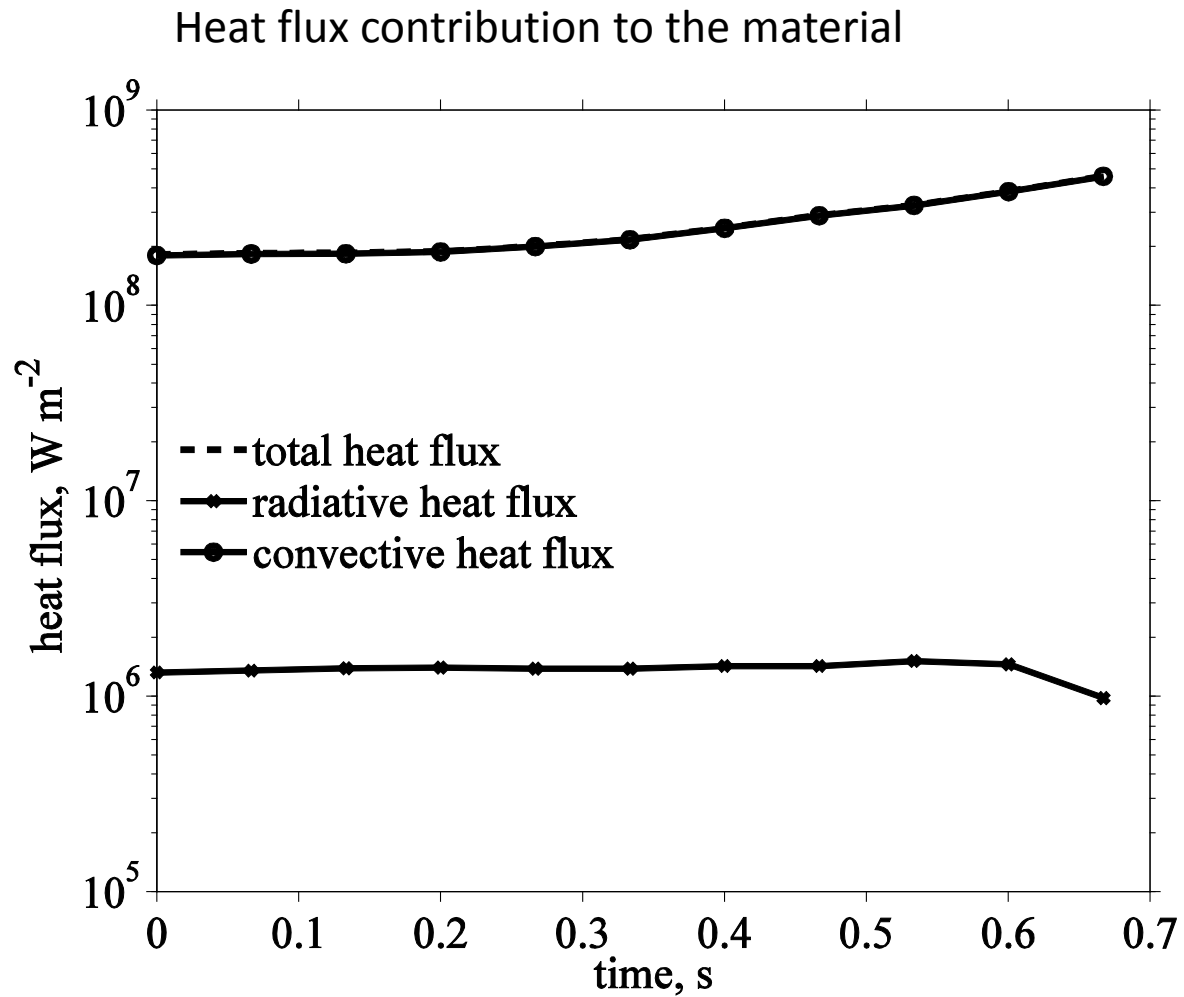
Animation of moving fronts



Melt layer



# Heat flux and mass removal from 60 to 50 km



# Outline

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- **Conclusion and Future Work**

# Conclusion

- Tools developed at VKI for spacecraft entries have been adapted and applied to meteor entry applications:
  - The ablative boundary condition was developed with an approach similar to re-entry vehicles
  - Melting phenomenon was included to the gas-surface interaction model
  - The material and flow solver were coupled through an implicit procedure
  
- Important results have been obtained using engineering tools:
  - The initial conditions for the flow solver are very important
  - The melting layer remains very thin due to a high mass removal
  - Decrease of the melting layer along the trajectory
  - The major source of mass lost is through mechanical removal
  - Radiative heat flux is much smaller than convective contribution

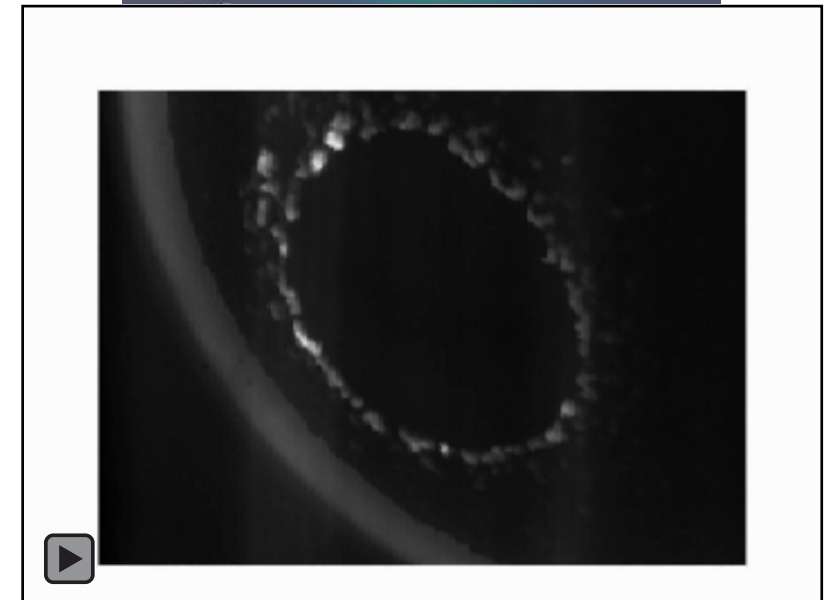
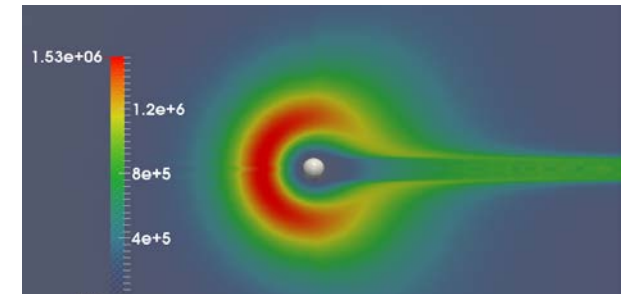
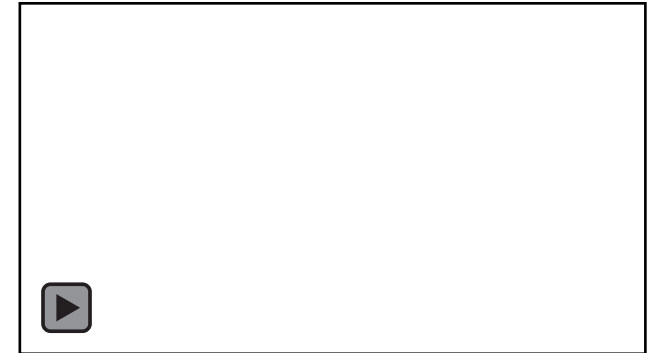
# On-going work

- Study of the meteor ablation in the Argo solver<sup>2</sup> and comparison with experimental results
- Development of DSMC tools for rarefied regimes<sup>3</sup> (Sparta simulation) (Federico talk)
- Experimental studies of real meteors in the Plasmatron<sup>1</sup> (Thierry talk)

<sup>1</sup> Zavalan, VKI RM (2016)

<sup>2</sup> Schroyen, PhD thesis (2016)

<sup>3</sup> Federico Bariselli, PhD student



# Development of evaporation and melting models for meteor phenomenon in the continuum regime

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